

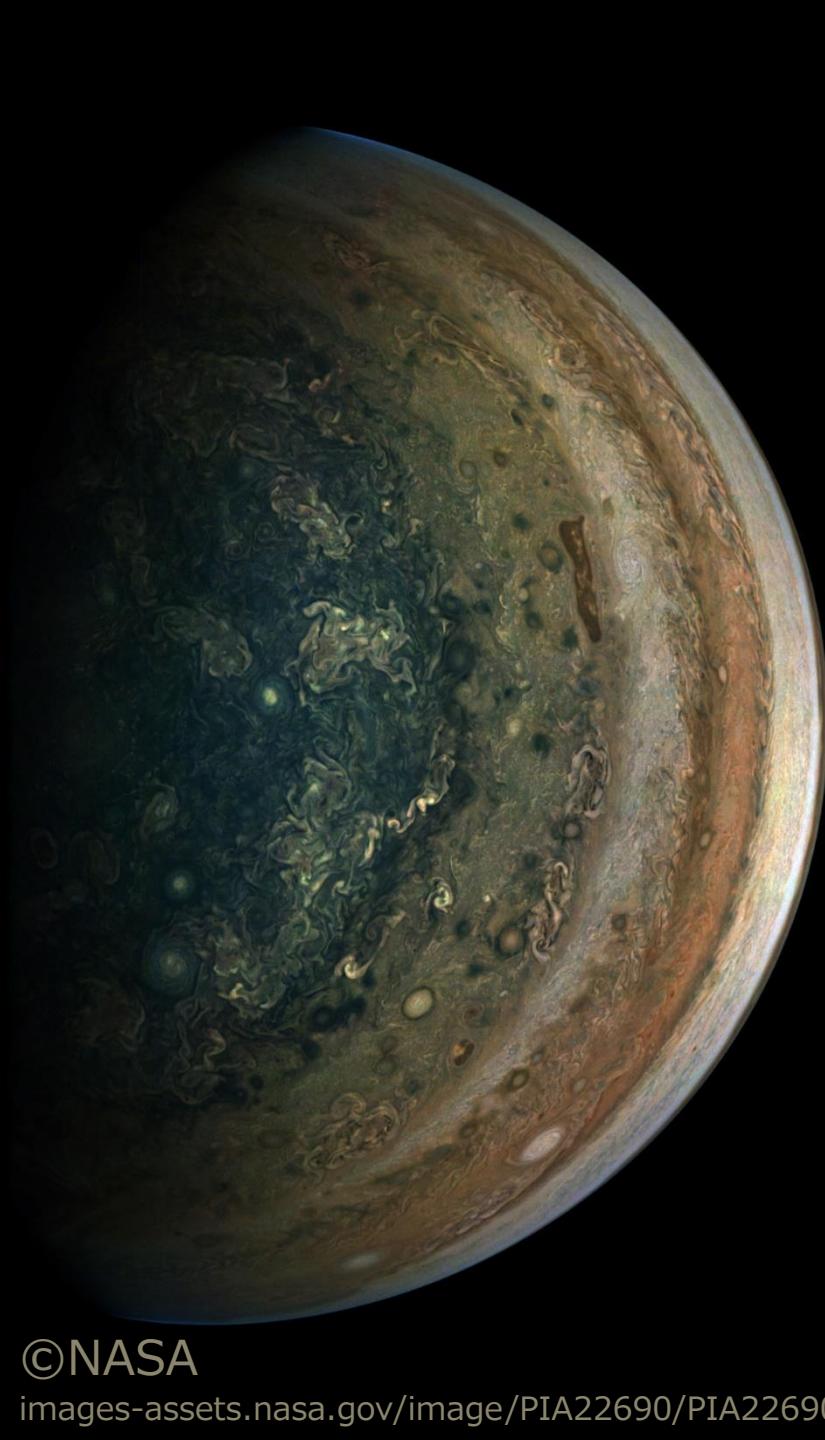
The 7th Mission Idea Contest Lecture Series
For Deep Space Science and Exploration



Deep Space Exploration and Micropropulsion

Hiroyuki Koizumi

- Associate Professor, The University of Tokyo
- CTO, Pale Blue Inc.



0: Preface

CommentScreen

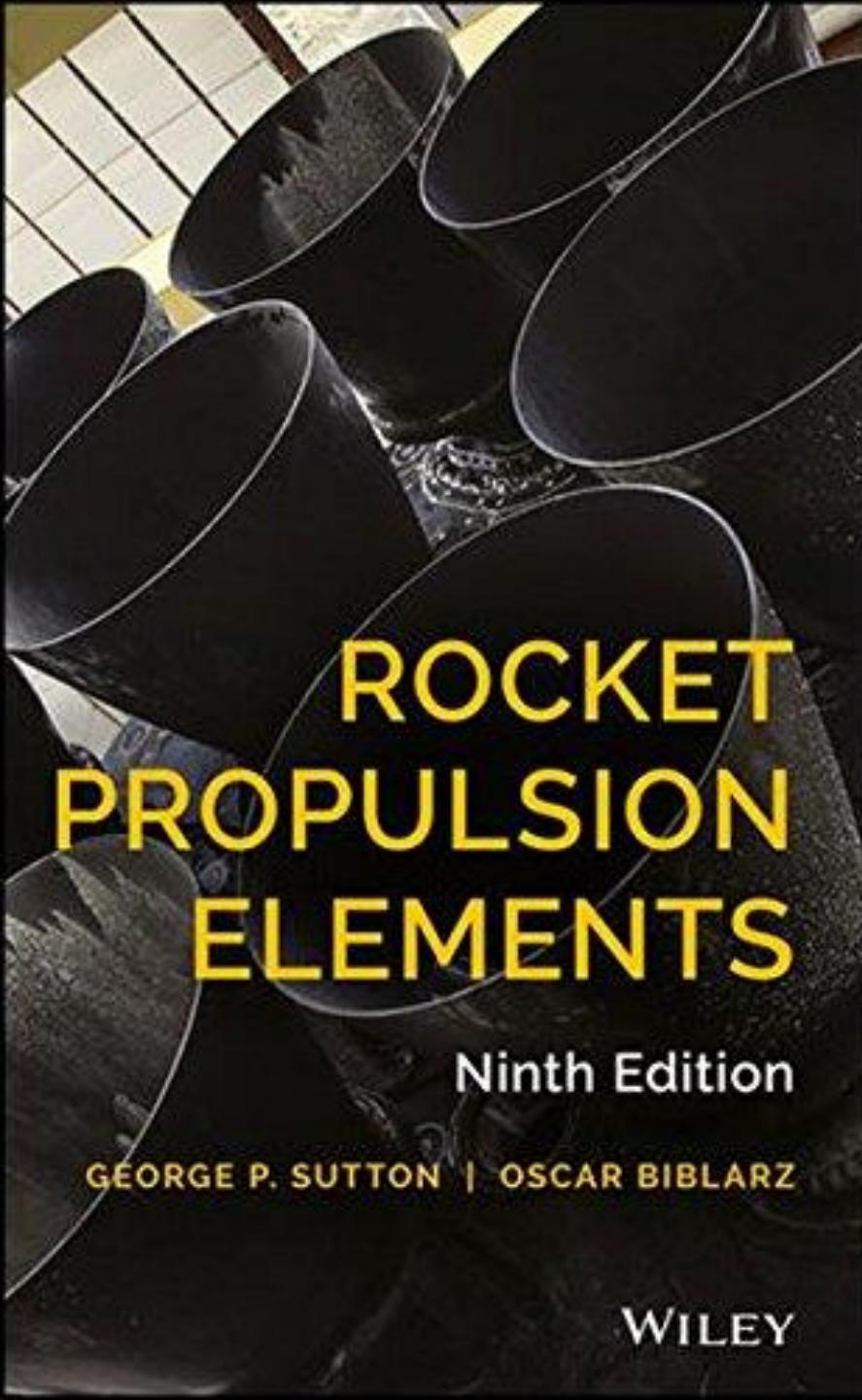
Anonymous comment app.

Freely input your question, comments, & impressions.

URL :
(check a chat)

<https://commentscreen.com/comments?id=IcjvccNIaUTKK9q6NqZh>





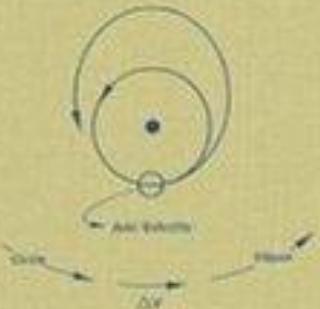
by G.P. Sutton & O. Biblarz

Classical & popular

Old but new (9th Edition)

Not recommend Jpn ver.
(old and expensive)

There is Kindle ver



CHARLES D. BROWN

Spacecraft Propulsion

by C. D. Brown

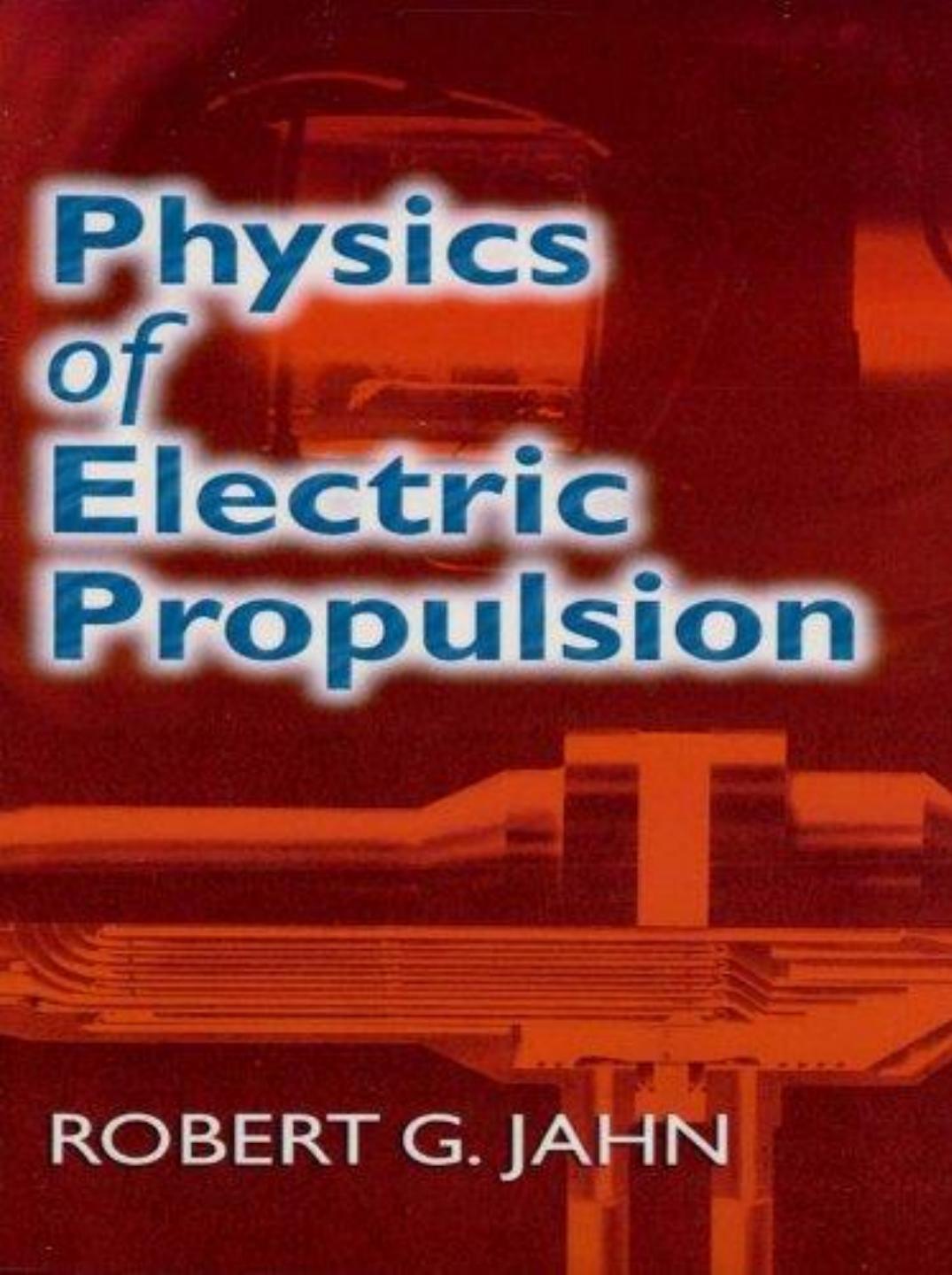
Chemical propulsion

- Mono-propellant
- Bi-propellant
- Solid rocket
- Cold-gas

AIAA

Education Series

J. S. PRZEMIENIECKI / SERIES EDITOR-IN-CHIEF



Physics of Electric Propulsion

ROBERT G. JAHN

by R.G. Jahn

Classical & popular

Technologically Old,
but long seller =
good book

There are Paper back
ver & Kindle ver

Fundamentals of Electric Propulsion

Ion and Hall Thrusters

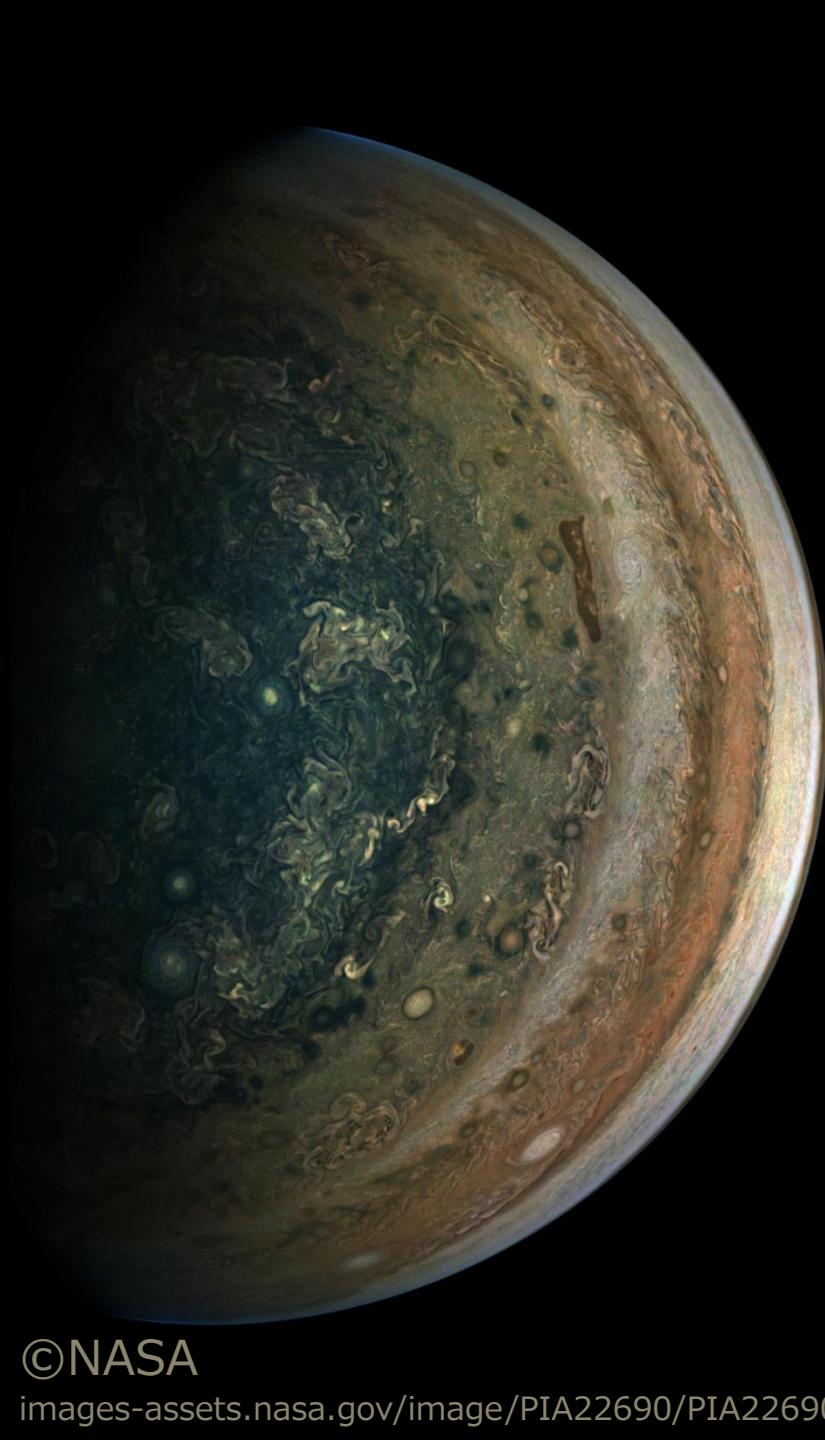


Dan M. Goebel
Ira Katz

by D.M. Goebel & I. Katz

Technologically new

Focusing on ion/Hall
thruster

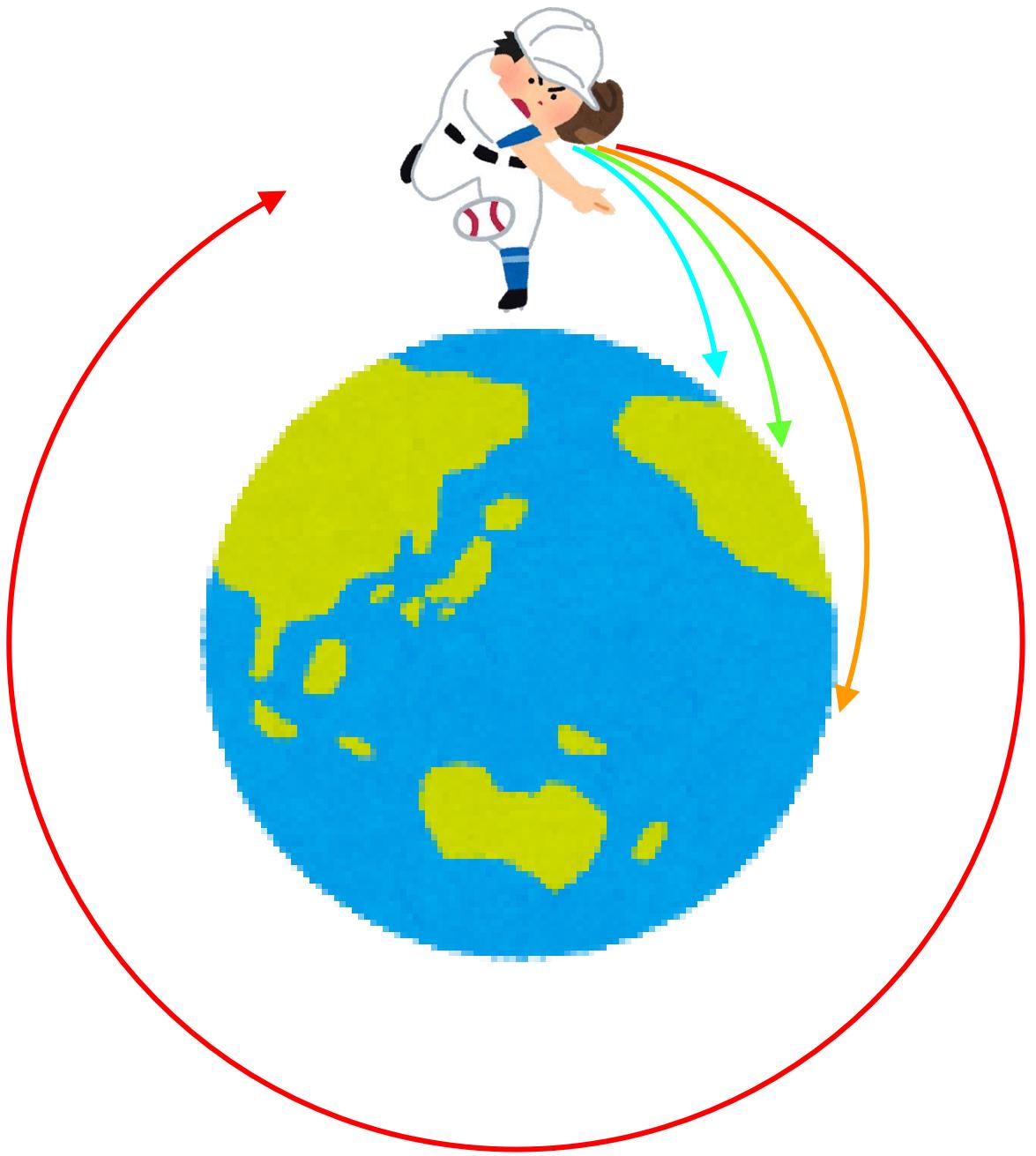


1: Fundamentals

- 2: Chemical Propulsion
- 3: Electric Propulsion
- 4: Micropropulsion

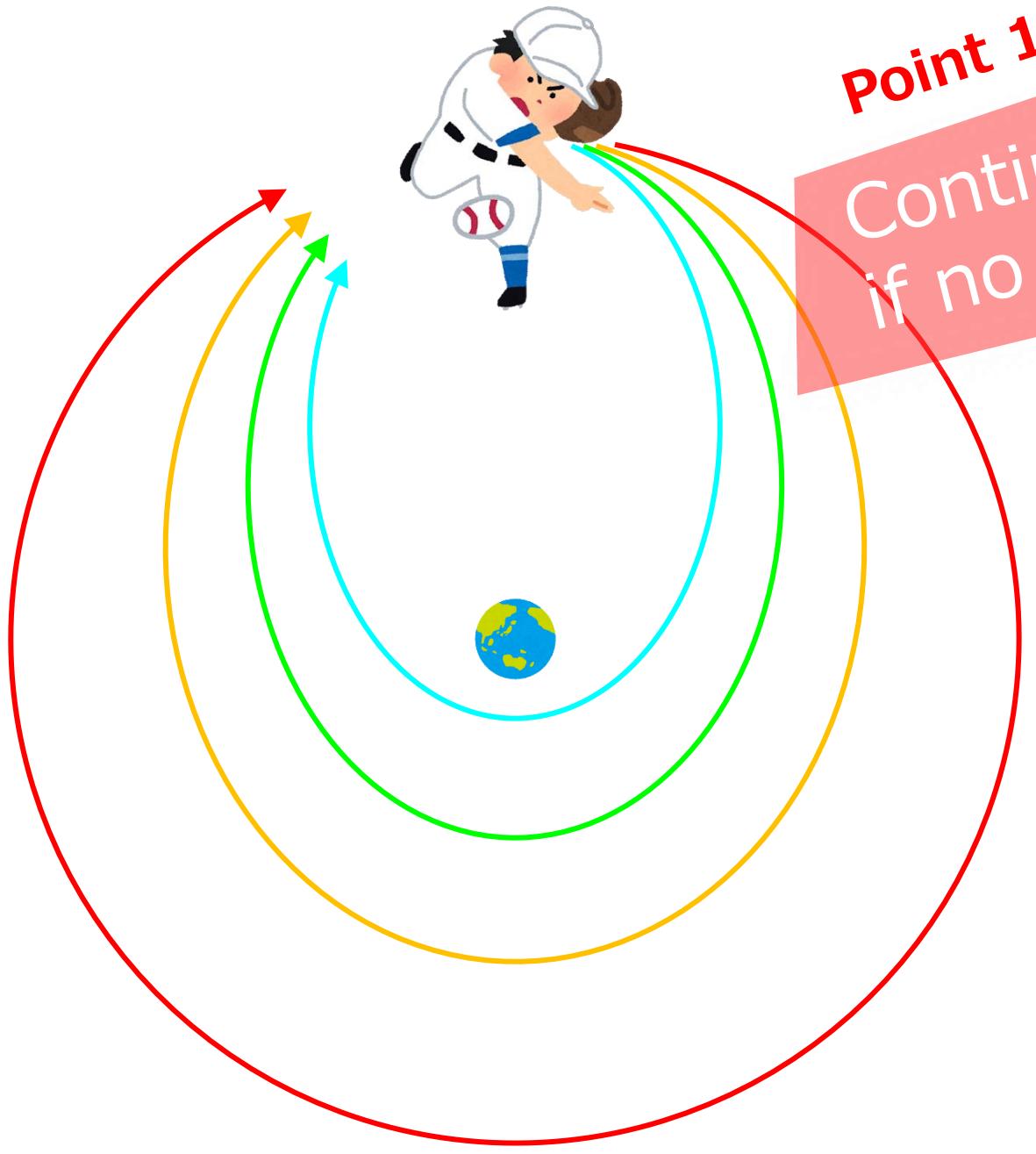


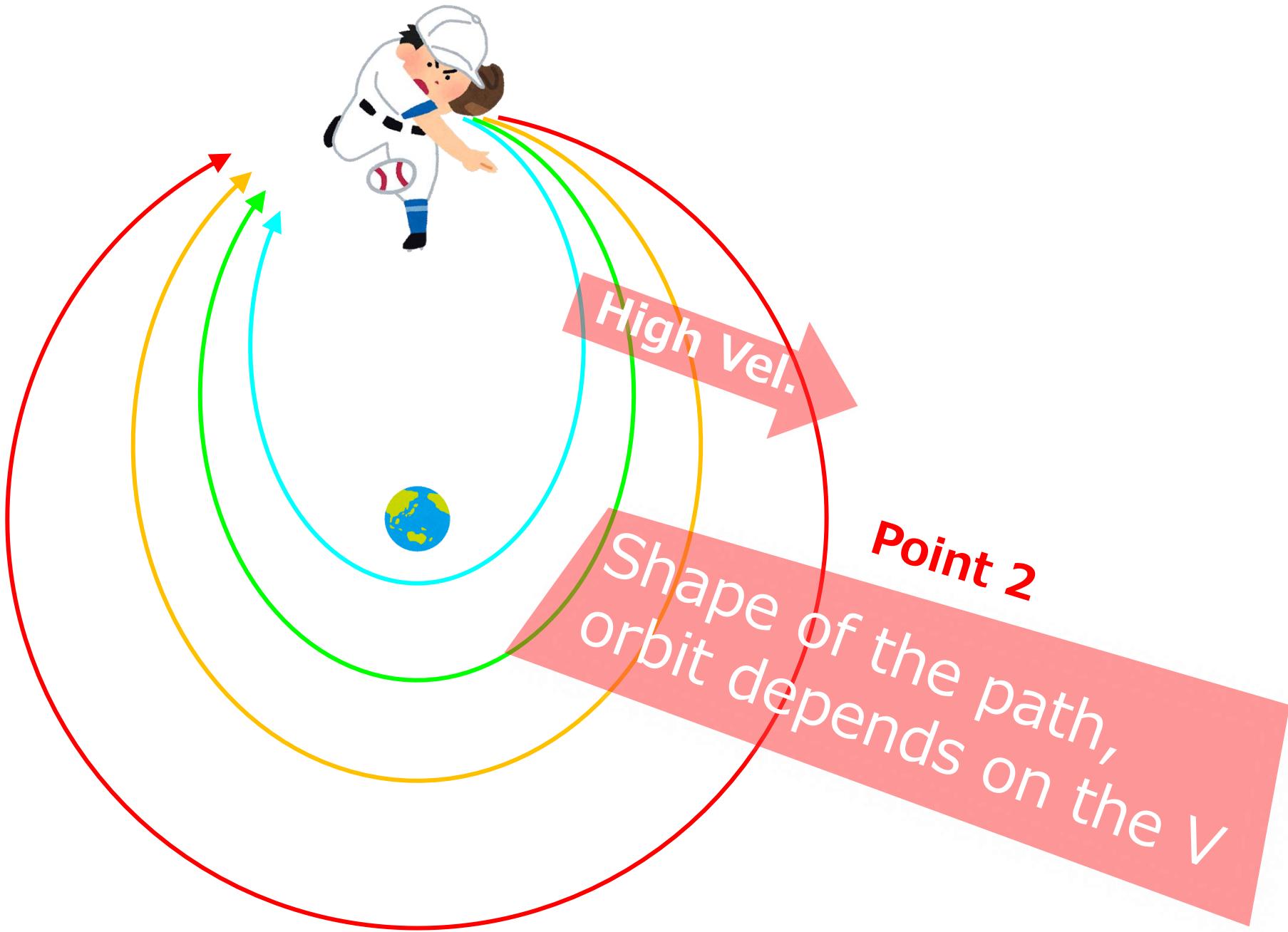
Just falling
Going to the center by energy loss



Point 1

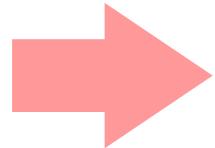
Continue to move
if no obstacle



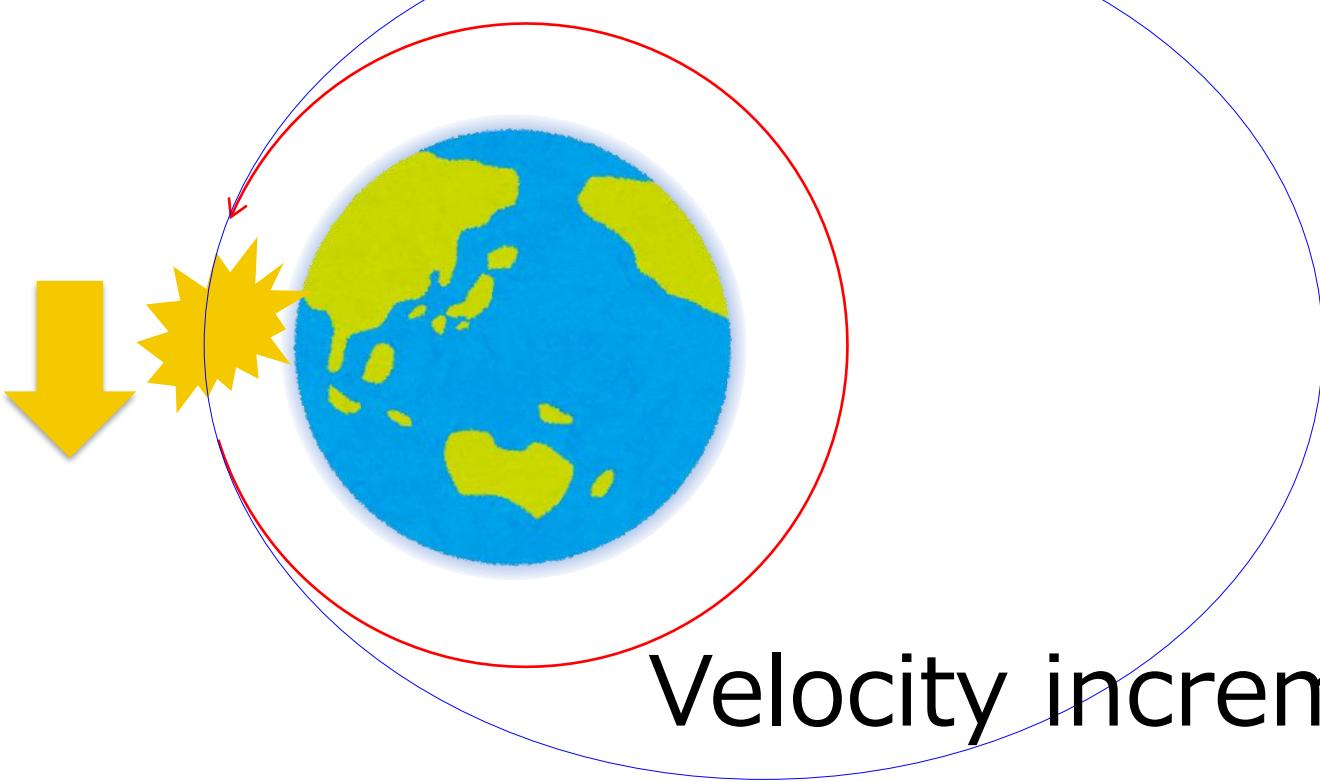


Velocity Increment: ΔV

How to change the orbit



Adding velocity (acceleration)



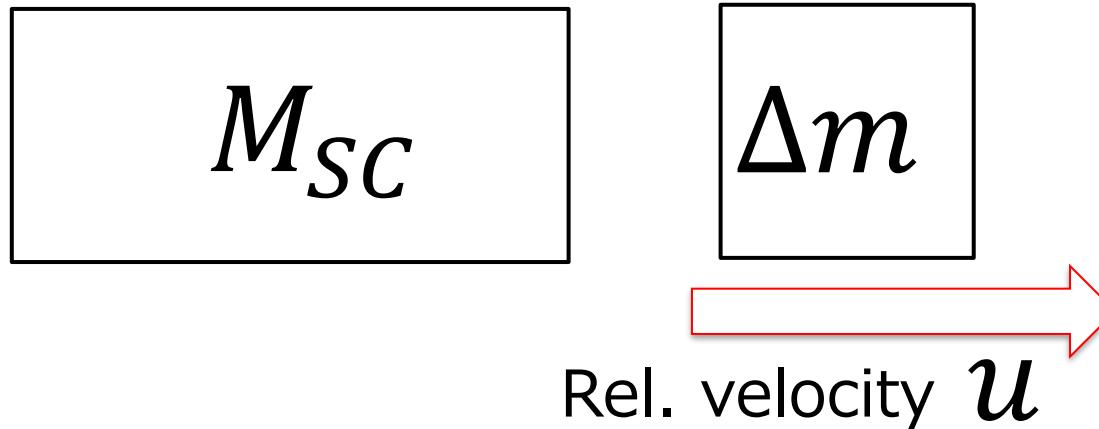
How to gain velocity?



Nothing
You need to bring something to push

How does a rocket work?

Mass Δm is released from a spacecraft at a velocity u in time Δt



Impulse = Momentum increment

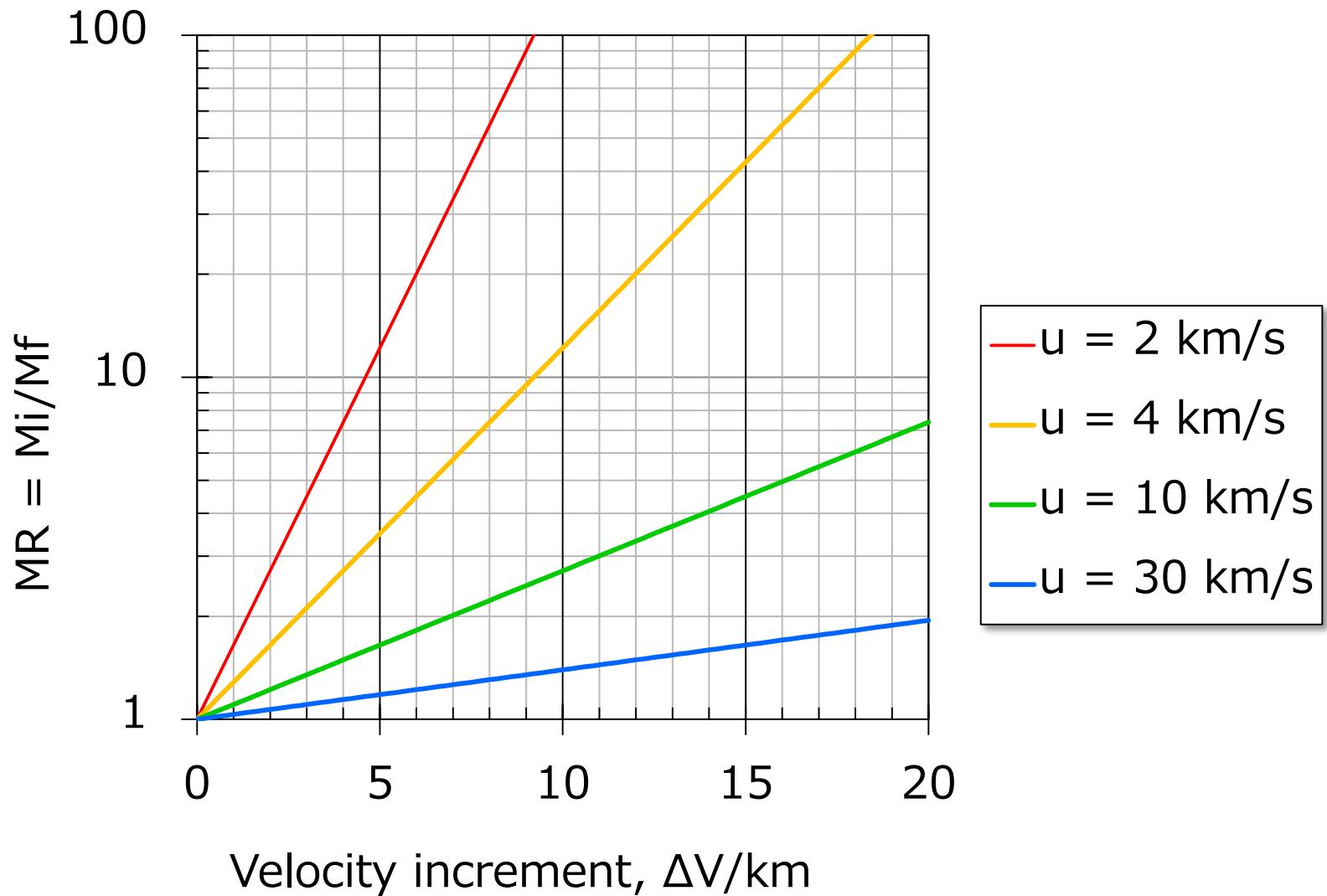
$$F\Delta t = \Delta m u$$

$$F = \dot{m} u \quad : \text{mass flow rate}$$

World's Launch Vehicles

Engine	Launcher	Propellant	Ex Vel.	Thrust
F1	Saturn V	LOX/RP-1	3.0 km/s	7.7 MN
RD-107	Soyuz	LOX/RP-1	3.1 km/s	1.0 MN
RD-264	Dnepr	N2O4/UDMH	3.2 km/s	4.5 MN
SSME	Shuttle	LOX/LH2	4.5 km/s	2.2 MN
LE7A	H2A	LOX/LH2	4.3 km/s	1.1 MN
Vulcain2	Arian 5	LOX/LH2	4.3 km/s	1.3 MN
SSRB	Shuttle	Composite	2.7 km/s	13.8 MN
SRB-A	H2A	Composite	2.8 km/s	2.3 MN
M-V-1	M-V	Composite	2.8 km/s	2.4 MN

Exhaust velocity is a key



Propulsion = Energy converter

(Any → Kinetic energy)

✓ Chemical propulsion

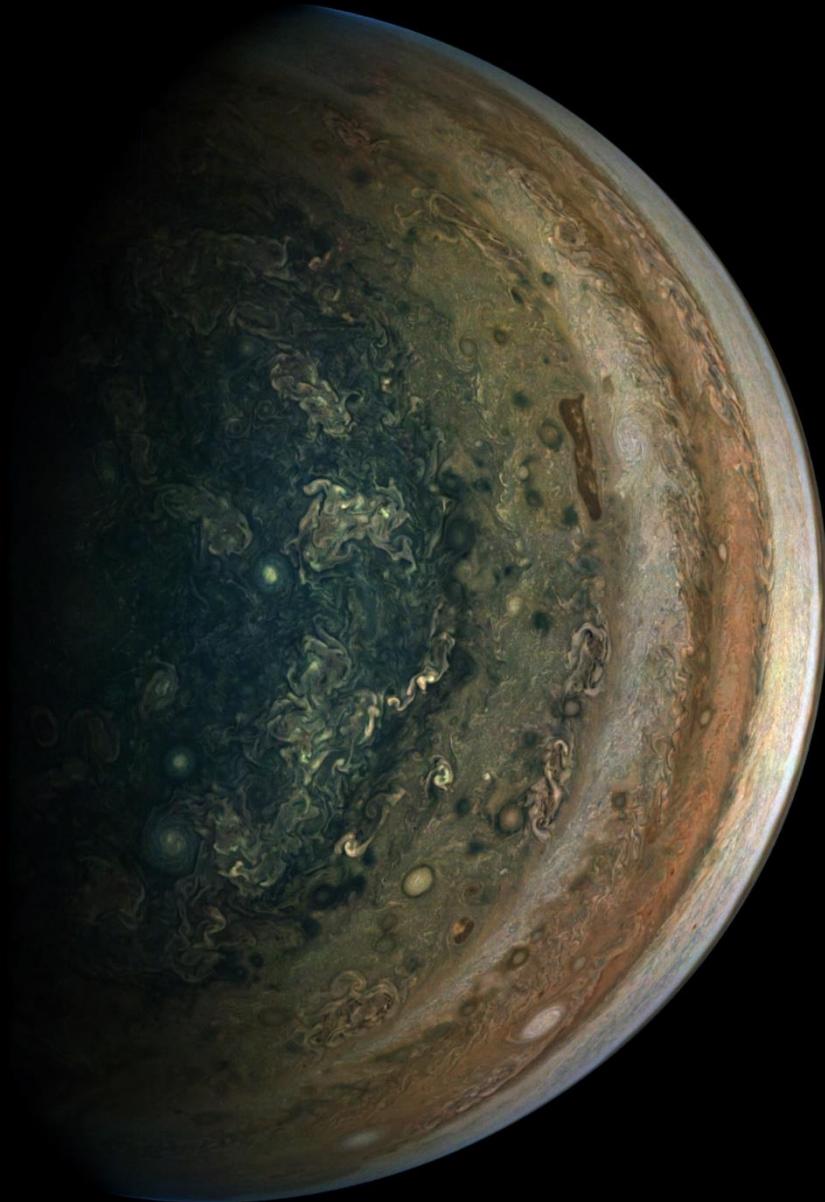
Chemical E → Kinetic E

Exhaust velocity : 1 – 4 km/s

✓ Electric propulsion

Electric E → Kinetic E

Exhaust : 10 – 50 km/s



1: Fundamentals

2: Chemical Propulsion

3: Electric Propulsion

4: Micropropulsion

Chemical Propulsion; Processes

Chemical energy

By combustion

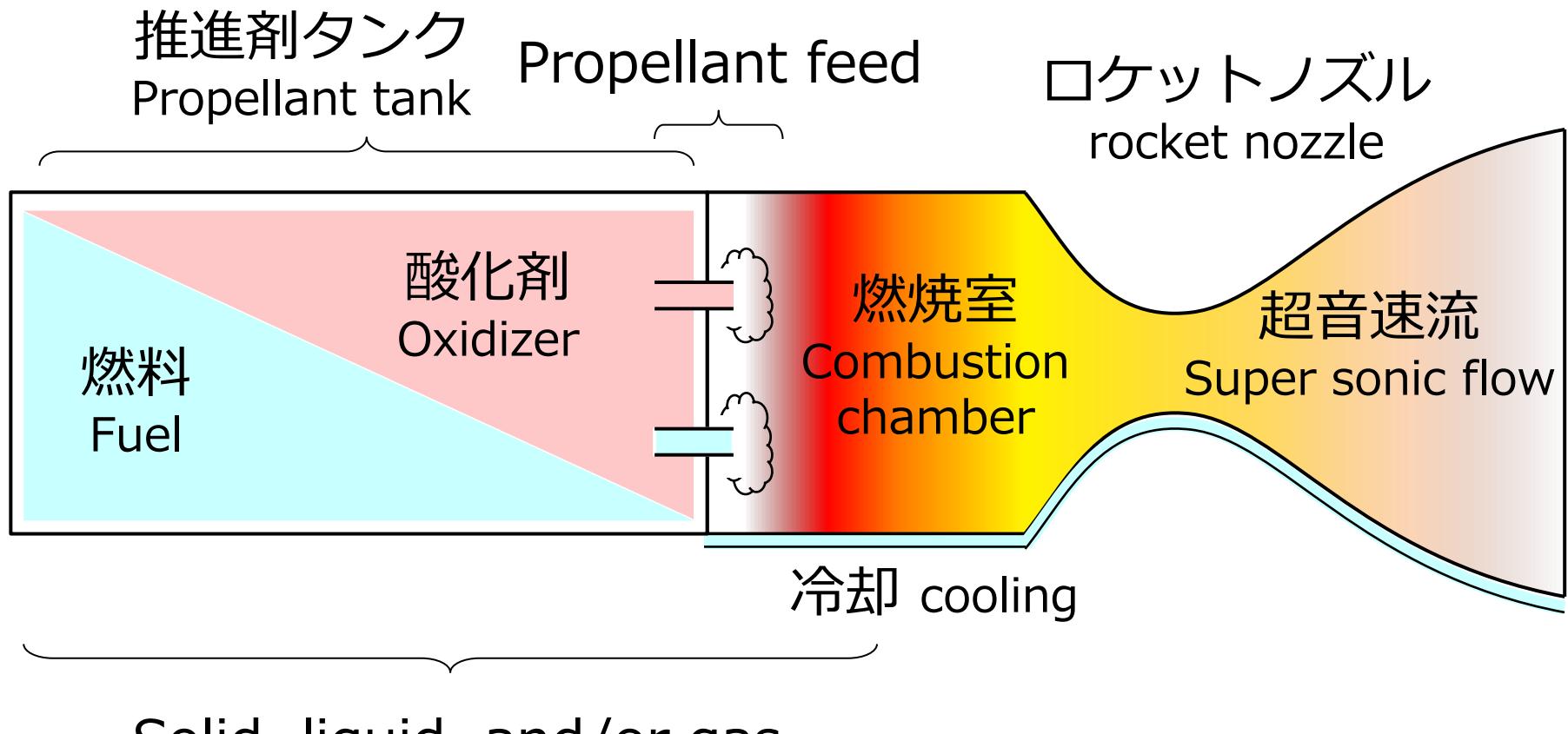
Thermal energy

Nozzle theory

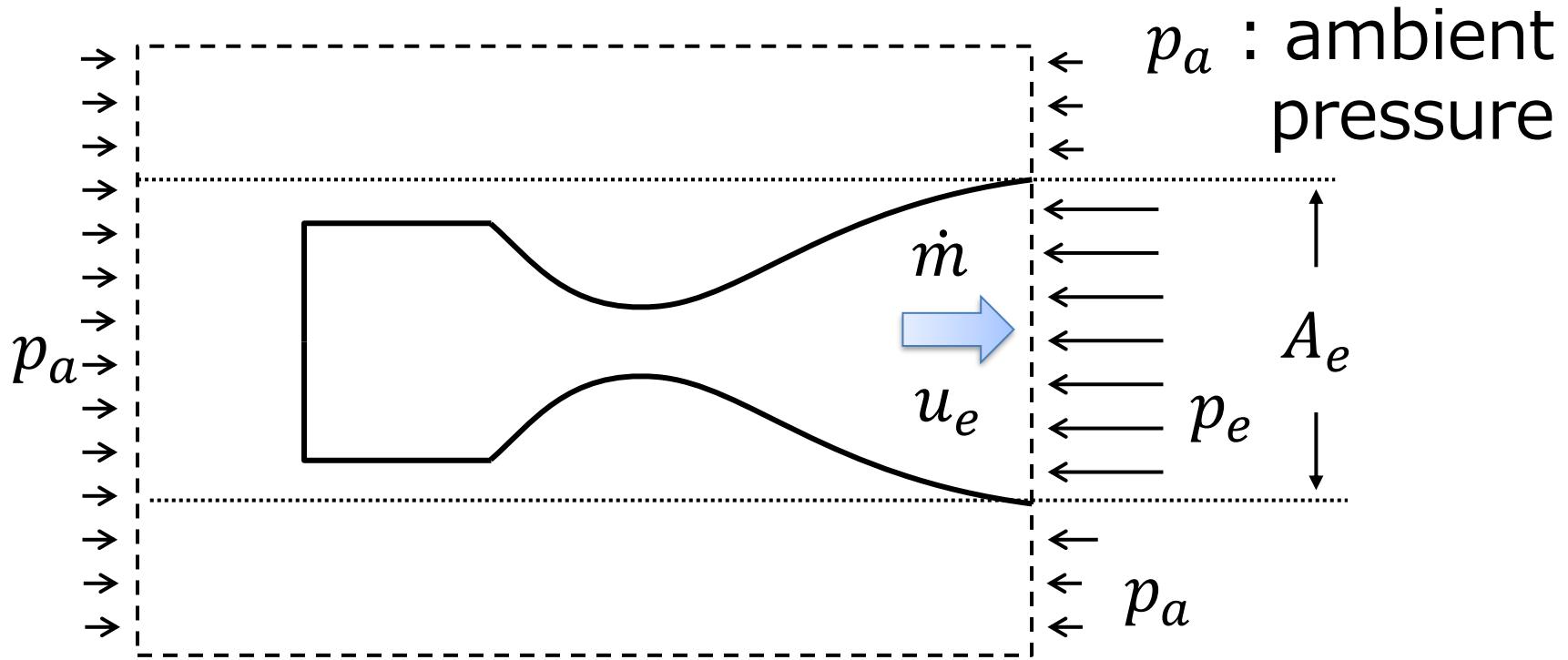
By a rocket-nozzle

Kinetic energy

Chemical Propulsion; Overview



Pressure thrust



Pressure difference of the front and back sides applies another thrust:

$$F = \dot{m}u_e + (p_e - p_a)A_e$$

Effective Exhaust Velocity

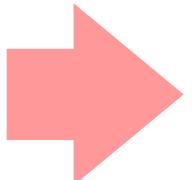
$$F = \dot{m}u_e + (p_e - p_a)A_e$$

…Actual “exhaust velocity” is not enough

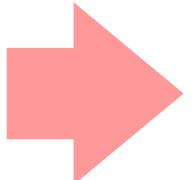
Introducing a new velocity: Effective Exhaust Velocity

$$c \equiv \frac{F}{\dot{m}}$$

Specific Impulse


$$I_{sp} \equiv \frac{F}{\dot{m}g} = \frac{FT}{\dot{m}Tg} = \frac{I}{Mg}$$

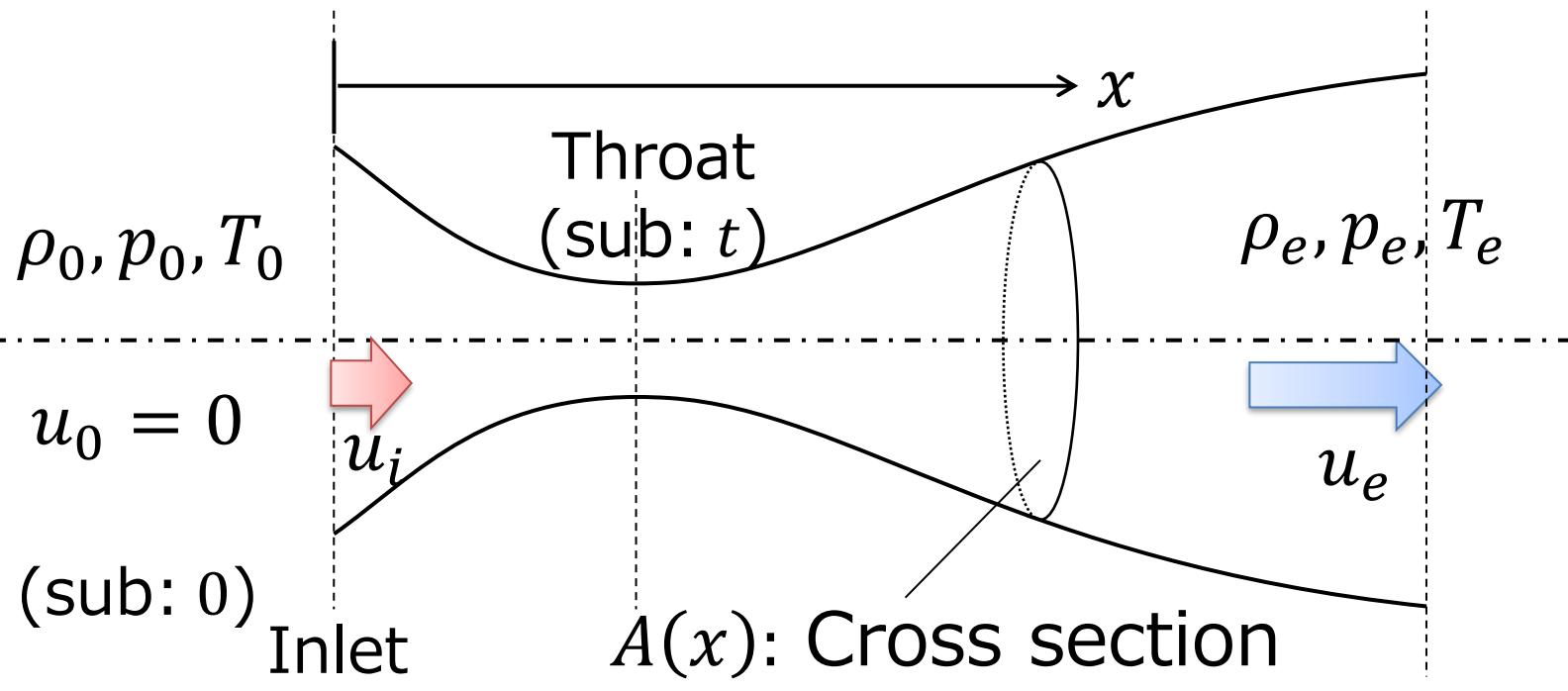
“ g ” is just by custom.


$$c = g I_{sp} \quad (\text{think about 10 times diff.})$$

e.g. $c = 4000 \text{ m/s}$ $I_{sp} = 408 \text{ s}$

$$c = 30000 \text{ m/s} \quad I_{sp} = 3060 \text{ s}$$

Rocket Nozzle; Quasi-1D & Isotropic



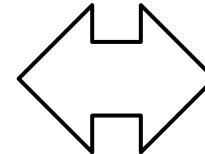
Flow parameters

$\rho = \rho(x)$: Density	Exit
$u = u(x)$: Velocity	(sub: e)
$p = p(x)$: Pressure	
$T = T(x)$: Temperature	

Government Equations

Mass conservation

$$d(\rho u A) = 0 \quad \cdots \text{Eq.(1)}$$



Unknowns

$$\begin{aligned} u &= u(x) \\ \rho &= \rho(x) \\ p &= p(x) \\ T &= T(x) \end{aligned}$$

Momentum conservation

$$d(\rho u^2 A) = -Adp \quad \cdots \text{Eq.(2)}$$

Energy conservation

$$c_v dT + pd \left(\frac{1}{\rho} \right) = 0 \quad \cdots \text{Eq.(3)}$$

Equation of state

$$p = R\rho T \quad \cdots \text{Eq.(4)}$$

Rocket-nozzle thrust

$$\begin{aligned} F &= \dot{m}u_e + (p_e - p_a)A_e \\ &= A_t p_0 \sqrt{\frac{2\gamma^2}{\gamma-1} \left(\frac{2}{\gamma+1}\right)^{\frac{\gamma+1}{\gamma-1}} \left\{ 1 - \left(\frac{p_e}{p_0}\right)^{\frac{\gamma-1}{\gamma}} \right\} + (p_e - p_a)A_e} \\ &= A_t p_0 C_F \end{aligned}$$

$$C_F = \sqrt{\frac{2\gamma^2}{\gamma-1} \left(\frac{2}{\gamma+1}\right)^{\frac{\gamma+1}{\gamma-1}} \left\{ 1 - \left(\frac{p_e}{p_0}\right)^{\frac{\gamma-1}{\gamma}} \right\} + \left(\frac{p_e}{p_0} - \frac{p_a}{p_0}\right) \frac{A_e}{A_t}}$$

C_F : Thrust coefficient, 推力係数

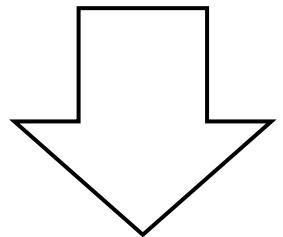
Depending on the aperture ratio and gas type

Expressing the acceleration of the gas by the nozzle

Exit Pressure & Aperture Ratio

Mass conservation between throat and exit

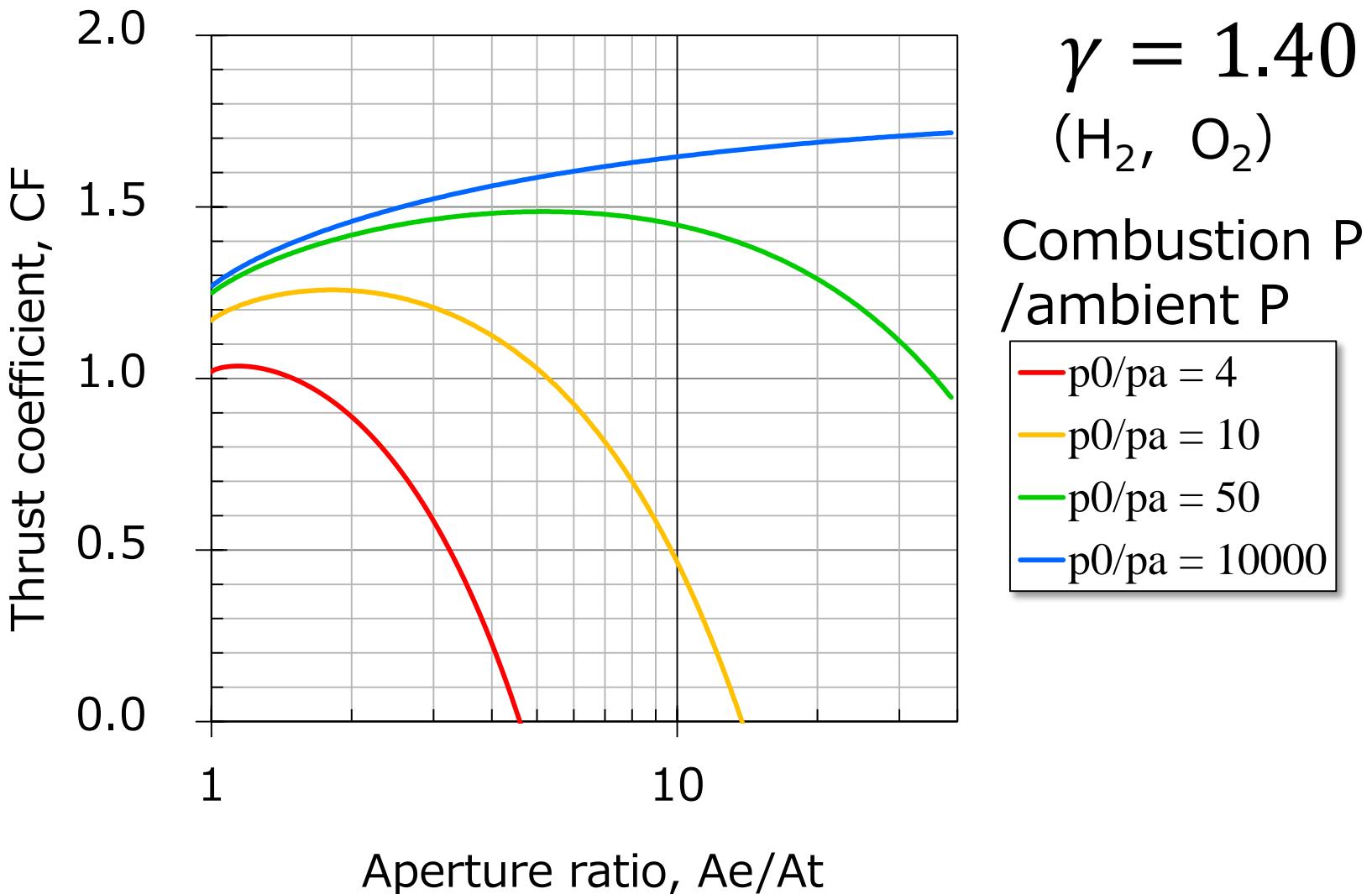
$$A_t p_0 \sqrt{\frac{\gamma}{RT_0}} \left(\frac{2}{\gamma + 1} \right)^{\frac{\gamma+1}{2(\gamma-1)}} = \rho_e u_e A_e$$



$$u_e = \sqrt{\frac{2\gamma}{\gamma - 1} RT_0 \left\{ 1 - \left(\frac{p_e}{p_0} \right)^{\frac{\gamma-1}{\gamma}} \right\}}$$

$$\frac{A_t}{A_e} = \left(\frac{\gamma + 1}{2} \right)^{\frac{1}{\gamma-1}} \left(\frac{p_e}{p_0} \right)^{\frac{1}{\gamma}} \sqrt{\frac{\gamma + 1}{\gamma - 1} \left\{ 1 - \left(\frac{p_e}{p_0} \right)^{\frac{\gamma-1}{\gamma}} \right\}}$$

Thrust Coefficient



$$\gamma = 1.40$$

($\text{H}_2, \text{ O}_2$)

Combustion P
/ambient P

- $p_0/\text{pa} = 4$
- $p_0/\text{pa} = 10$
- $p_0/\text{pa} = 50$
- $p_0/\text{pa} = 10000$

Rocket Thrust

$$\begin{aligned} F &= \dot{m}u_e + (p_e - p_a)A_e \\ &= A_t p_0 C_F \\ &= \dot{m}c^* C_F \end{aligned}$$

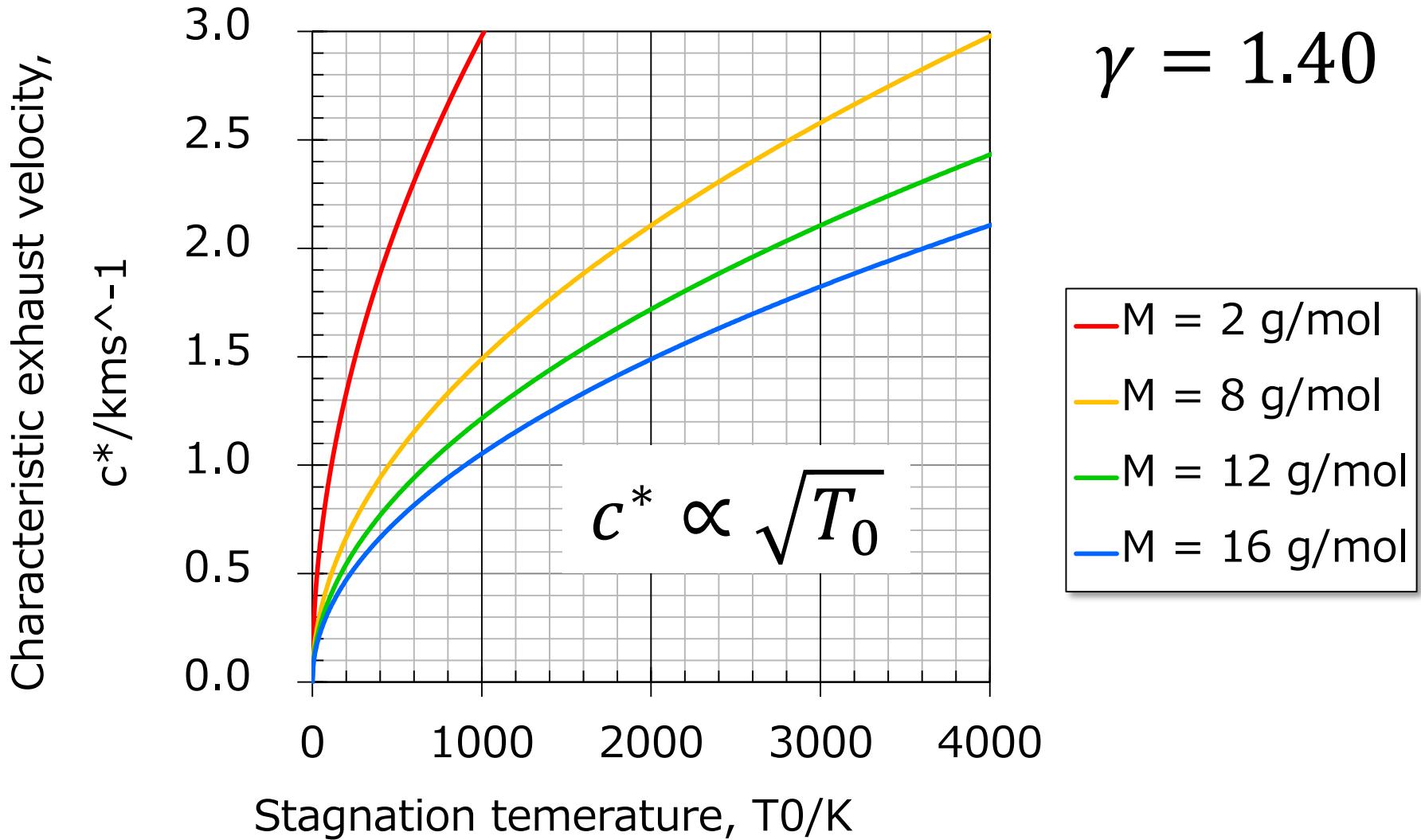
$$c^* \equiv \frac{A_t p_0}{\dot{m}} = \sqrt{\frac{RT_0}{\gamma} \left(\frac{\gamma + 1}{2} \right)^{\frac{\gamma+1}{\gamma-1}}}$$

c^* : Characteristic velocity (c star), 特性速度

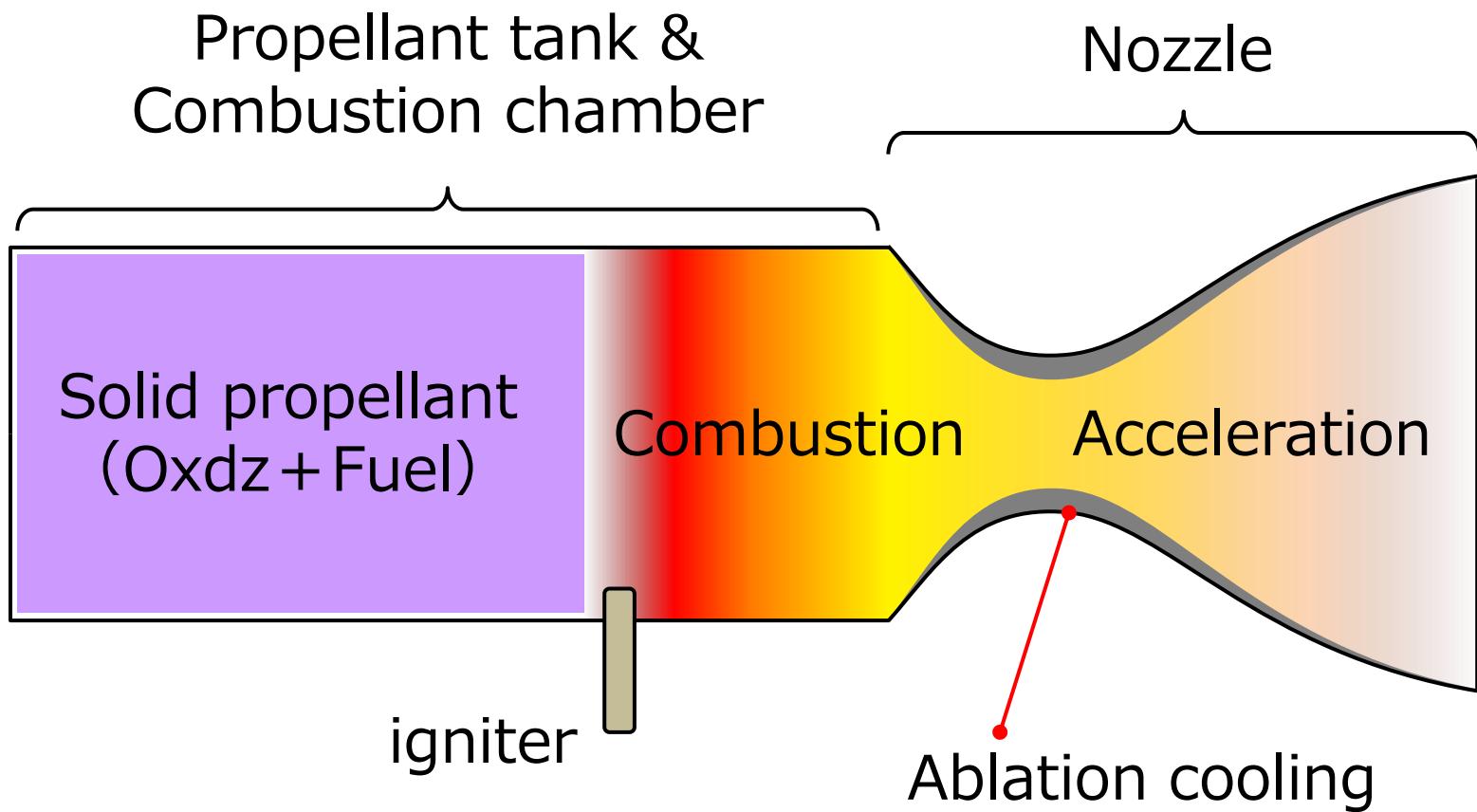
Depending on the temperature and gas type

Expressing the performance of combustion chamber

Characteristic Velocity



Solid motor; Structure



Double-based propellant

- Nitroglycerin (NG, $C_3H_5(ONO_2)_3$) : Fuel&Oxidizer
→Liquid, Plasticizer, High reactivity, O rich
- Nitrocellulose (NC , $C_{12}H_{14}(ONO_2)_6O_4$) : Fuel&Oxidizer
→Solide, Binder, Stable, F rich

Composite

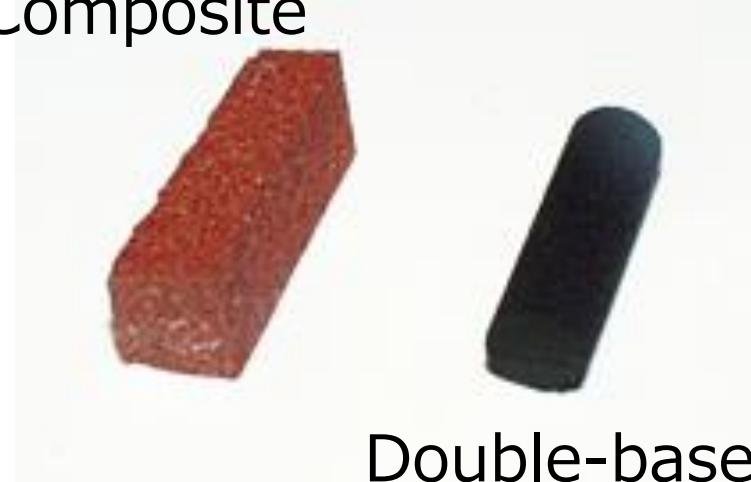


Double-based

Composite Propellant

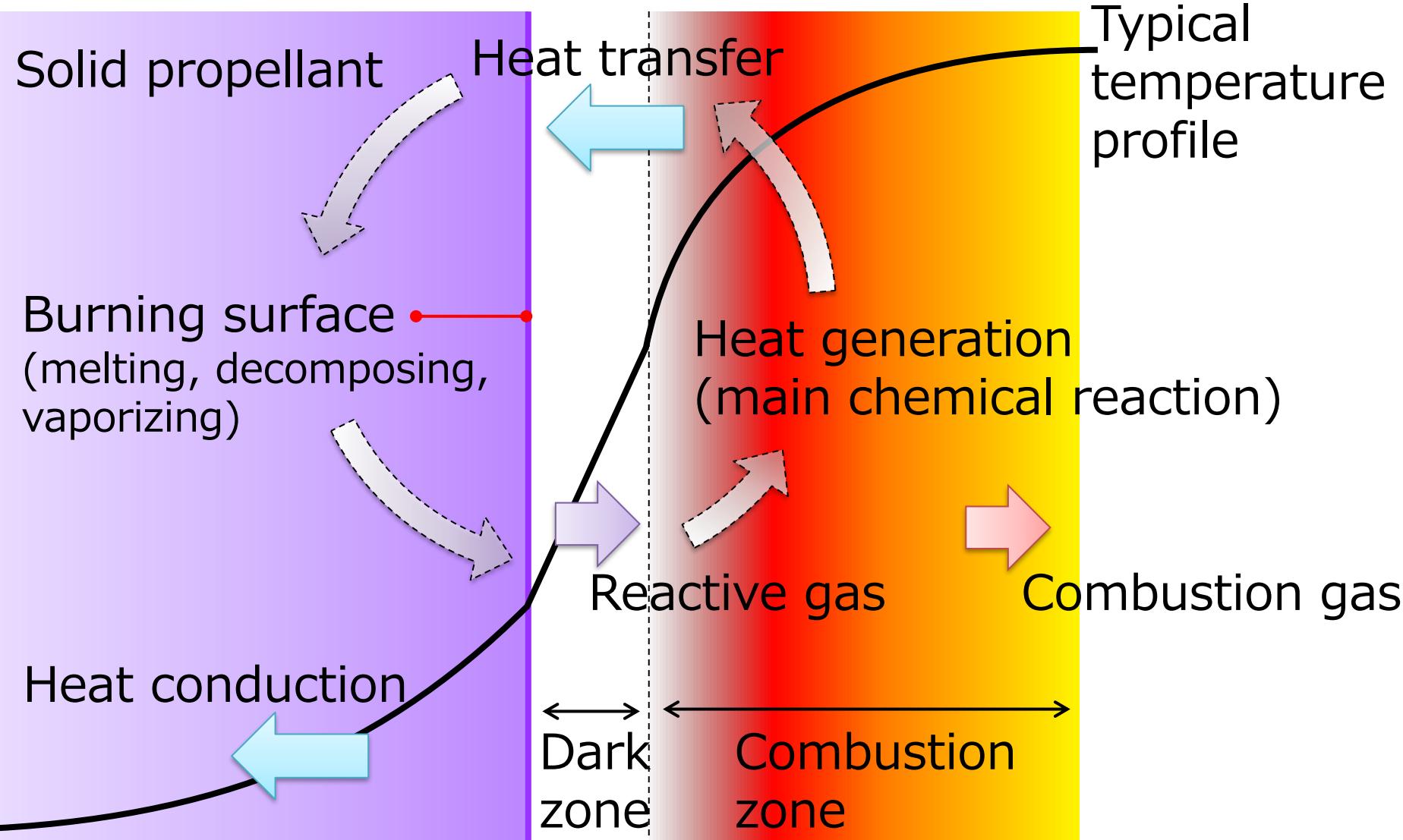
[Oxdzr : Ammonium perchlorate (AP) , etc
Fuel : Polymer, Binder, Polyvinyl Chloride (PVC) ,
Hydroxyl-terminated polybutadiene (HTPB) ,
Powdered metal (Al)

Composite



Double-based

Combustion structure (DB)



Burning Rate and Burning Area

Gas exhausted from the nozzle

$$\dot{m}_t = \frac{A_t P_c}{c^*}$$

Balance

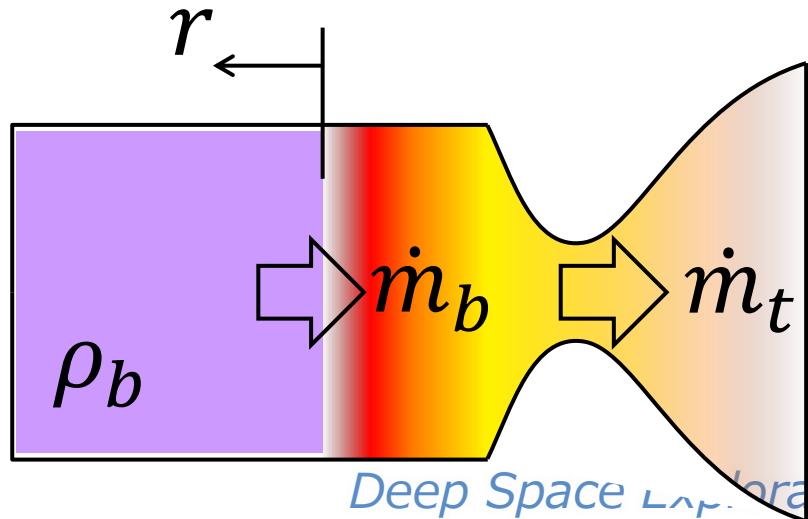
$$\dot{m}_t = \dot{m}_b$$

Gas generated by combustion

$$\dot{m}_b = \rho_b A_b r$$



$$P_c = \rho_b r c^* \frac{A_b}{A_t}$$



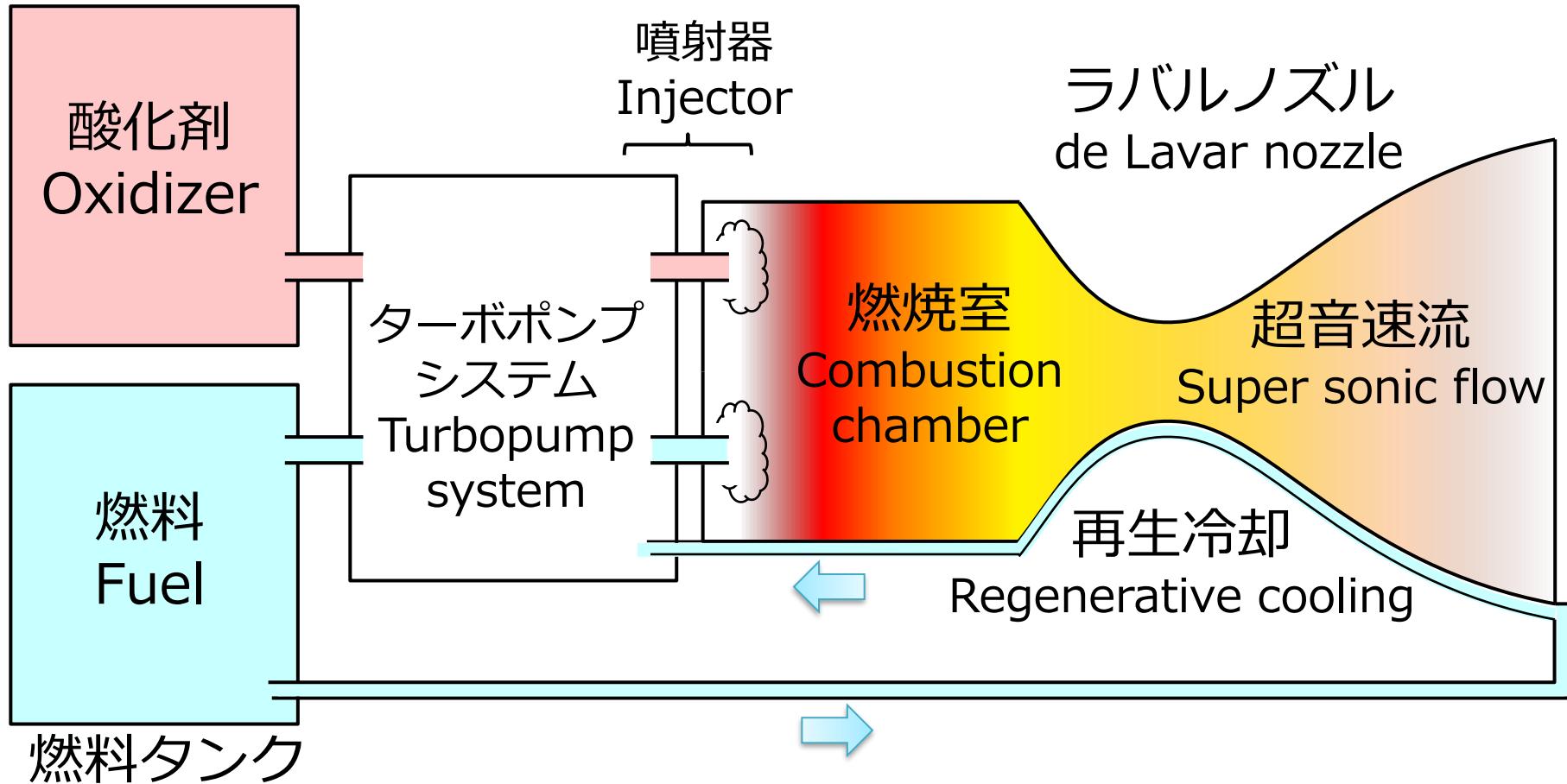
r : Burning rate (e.g. cm/s)

A_b : Burning area

ρ_b : Solid propellant density

Liquid Engine; Structure

酸化剤タンク
Oxidizer tank



燃料タンク
Propellant tank

Oxidizer

Oxygen (O₂)

Boiling point 90 K → specific gravity 1.14

LOX: Liquid Oxygen

The most popular as oxidizer

Nitrogen tetroxide, NTO (N₂O₄) ≈ MON

Boiling point 294 K → specific gravity 1.45

Popular by good storability

Hydrogen peroxide (H₂O₂)

Can be reacted using a catalyst

Red fuming nitric acid (RFNA: HNO₃+NO₂(5-20%))

Higher E than HNO₃. High toxicity

Fuel

Hydrogen (H₂)

Boiling point 20 K → Specific G 0.07 (low density)

Flammable in air

Low molecular mass, and high Isp

Hydrocarbon-based fuel (Kerosene, RP-1)

RP-1: highly refined for rocket engine

Boiling point 500 K, SG 0.81 (289K)

Good availability and good handling ability

Hydrazine (N₂H₄: CH1.97) , MMH, UDMH

Boiling point 387 K, SG 1.02 (293K)

Toxic, spontaneous combustion in air

Reaction using a catalyst (mono-propellant)

MMH:
Monomethylhydrazine

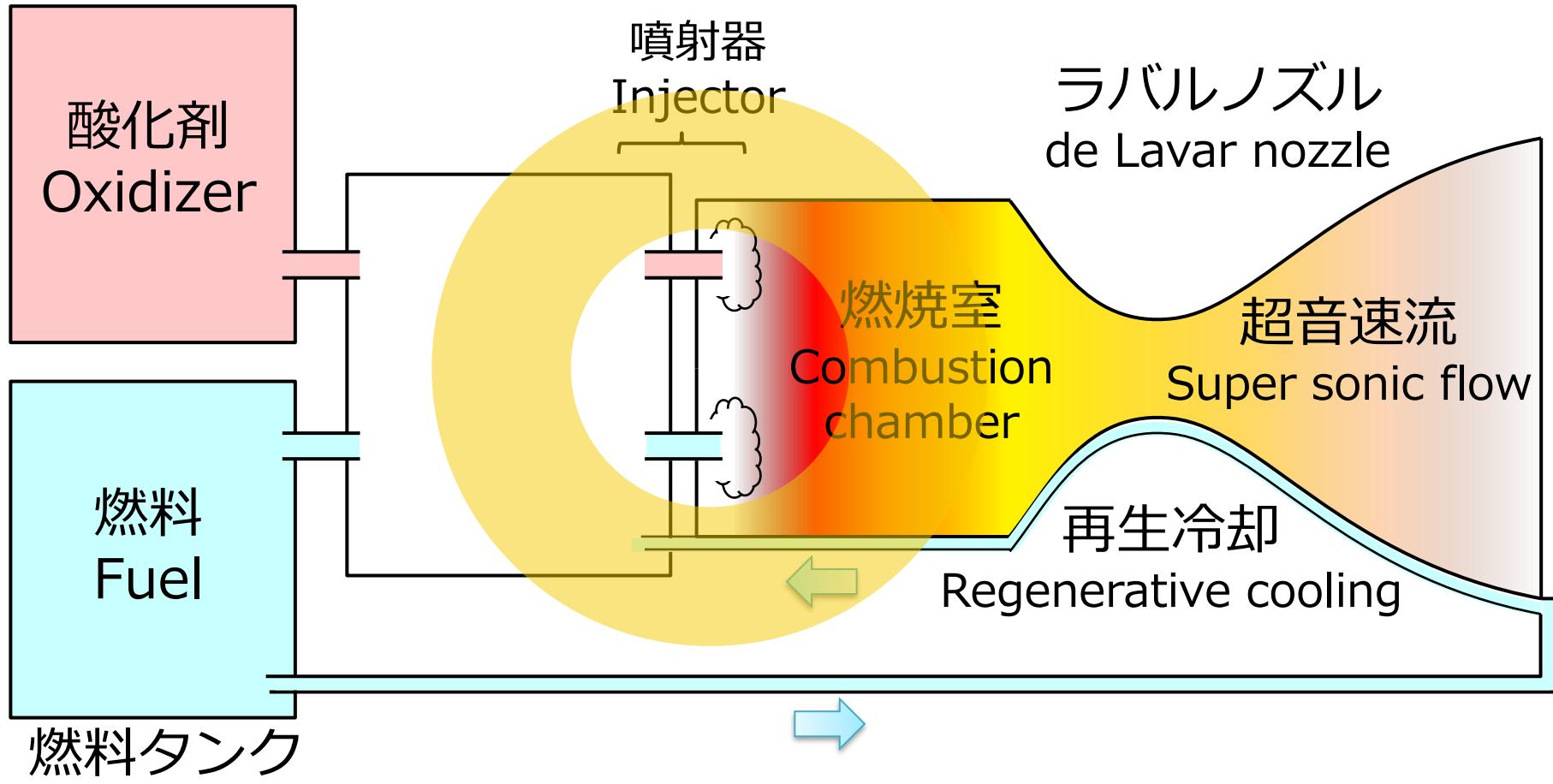
UDMH: unsymmetrical
dimethylhydrazine

C. Propulsion of Space Probes

	Fuel	Oxd.	#	Thrust/N
Bepicolombo (MPO)	MMH	N2O4	8	5 & 22
Hayabusa1/2	Hydrazine	N2O4	8	20
Mars Global Surveyor	Hydrazine	N2O4	13	4.4 & 600
Galileo	MMH	N2O4	13	10 & 400
Shuttle RCS	MMH	N2O4	44	110 & 3870
Viking Orbiter	MMH	N2O4	1	1330

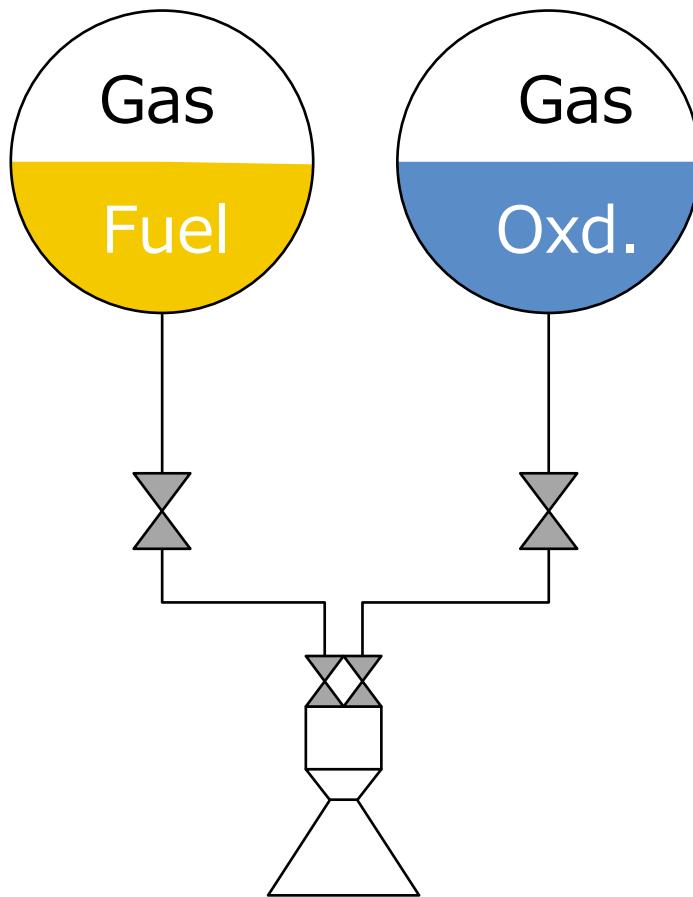
Liquid Engine; Structure

酸化剤タンク
Oxidizer tank



燃料タンク
Propellant tank

Blow Down Feed System



High pressure gas
Inside the tanks

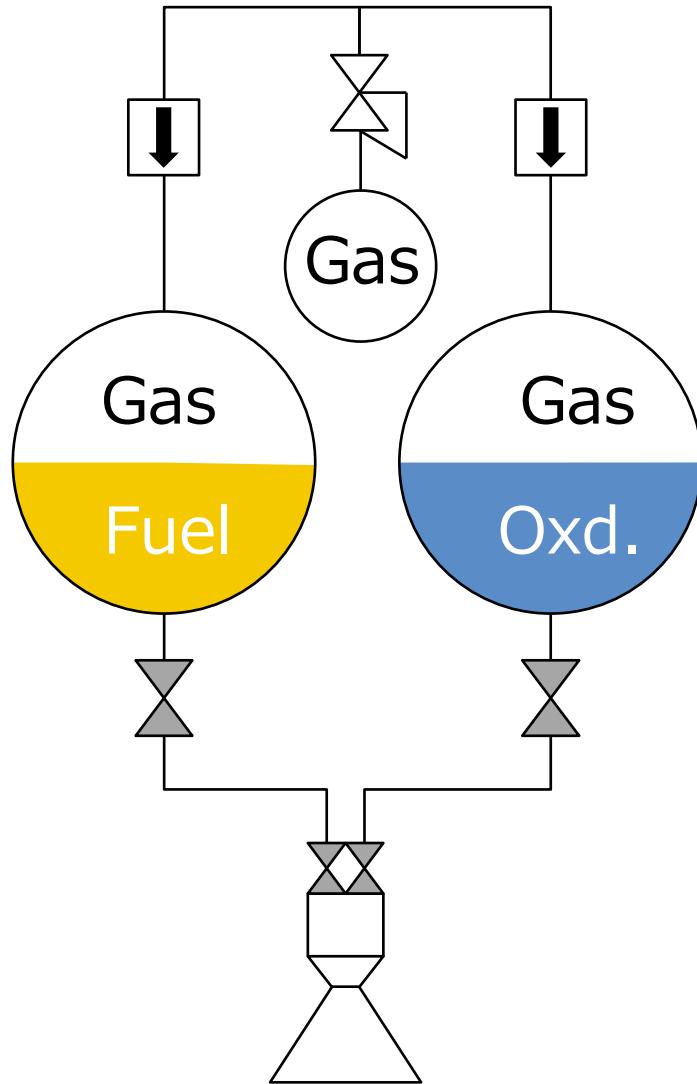


Pressure change
By the gas usage



Change of the flow rate

Gas Pressure Regulator System

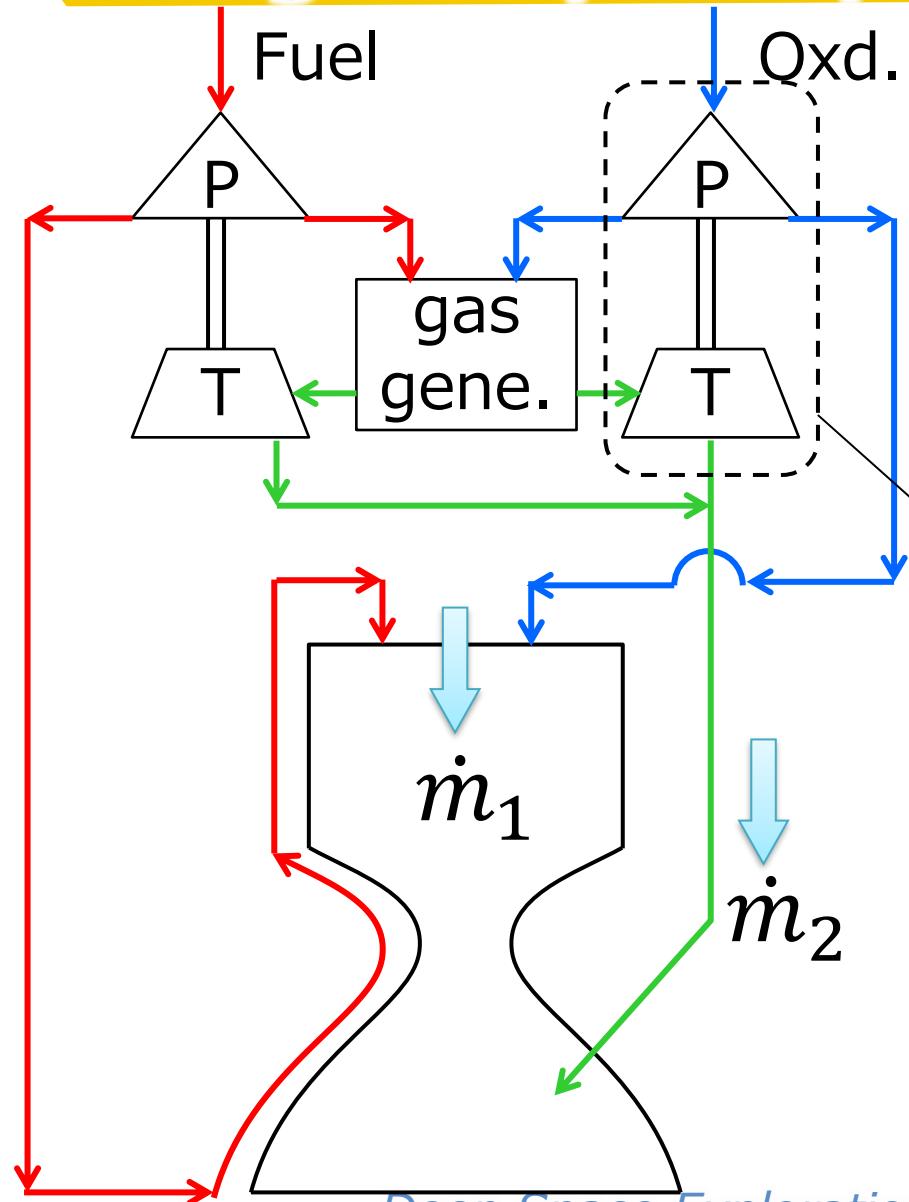


Pressure regulator

Reducing the input pressure of a fluid to a desired value at its output.



Engine Cycle System

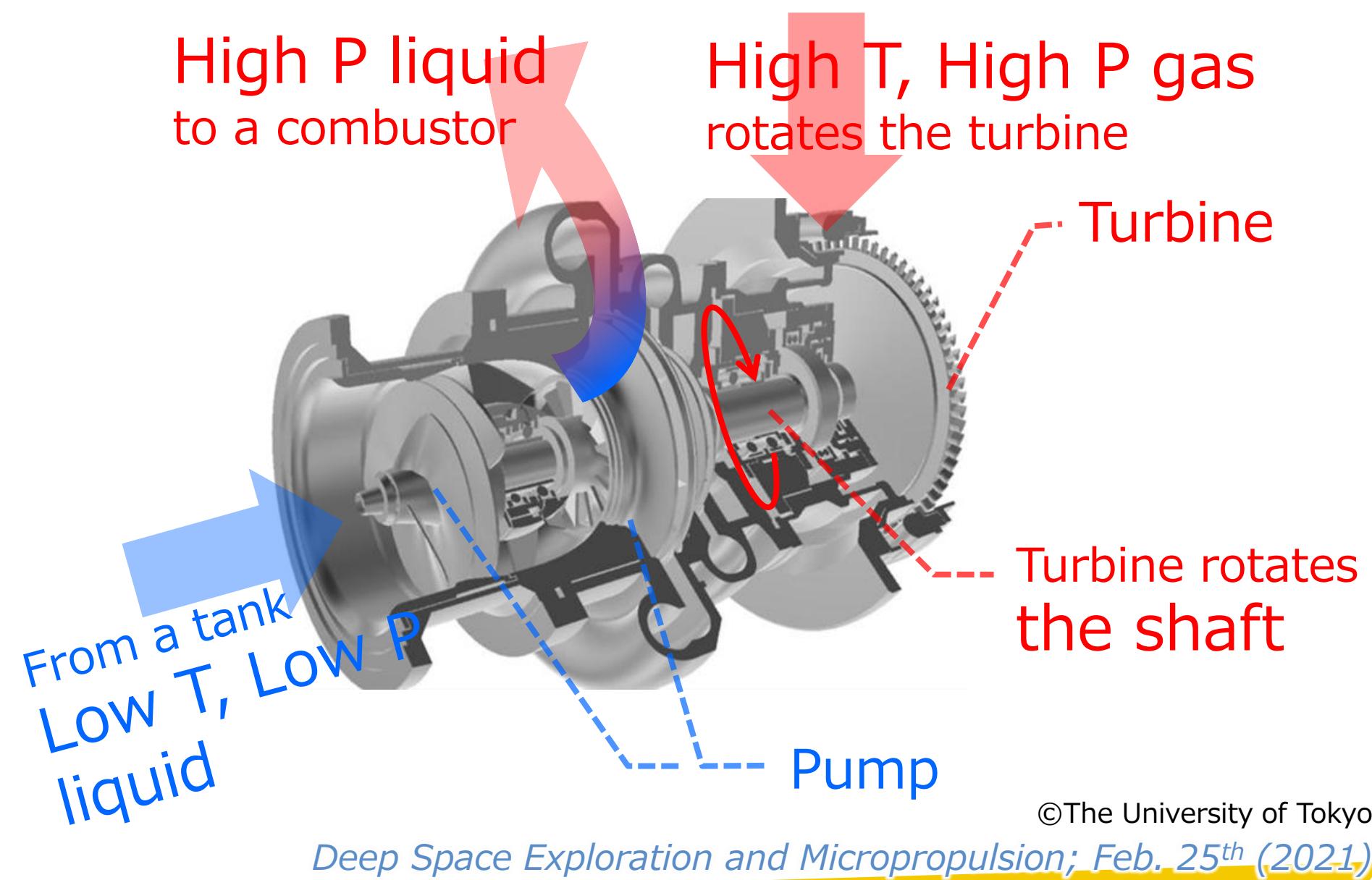


e.g. Gas generator Cycle

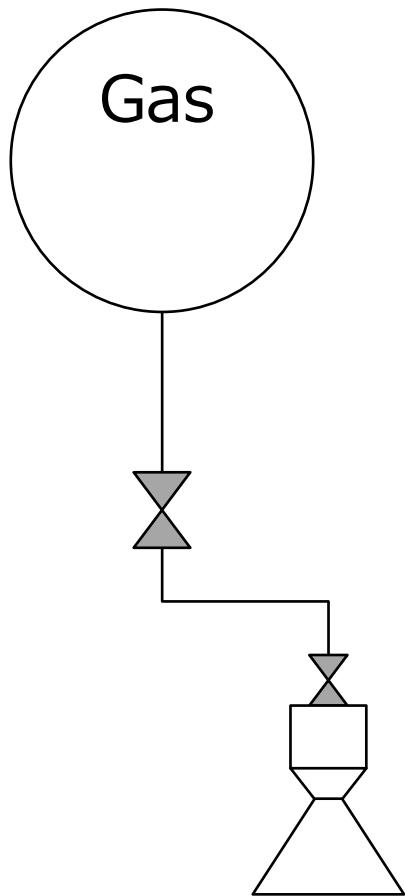
Pump and Turbine

Turbopump

Turbopump



Cold-gas Jet Thruster



The simplest thruster

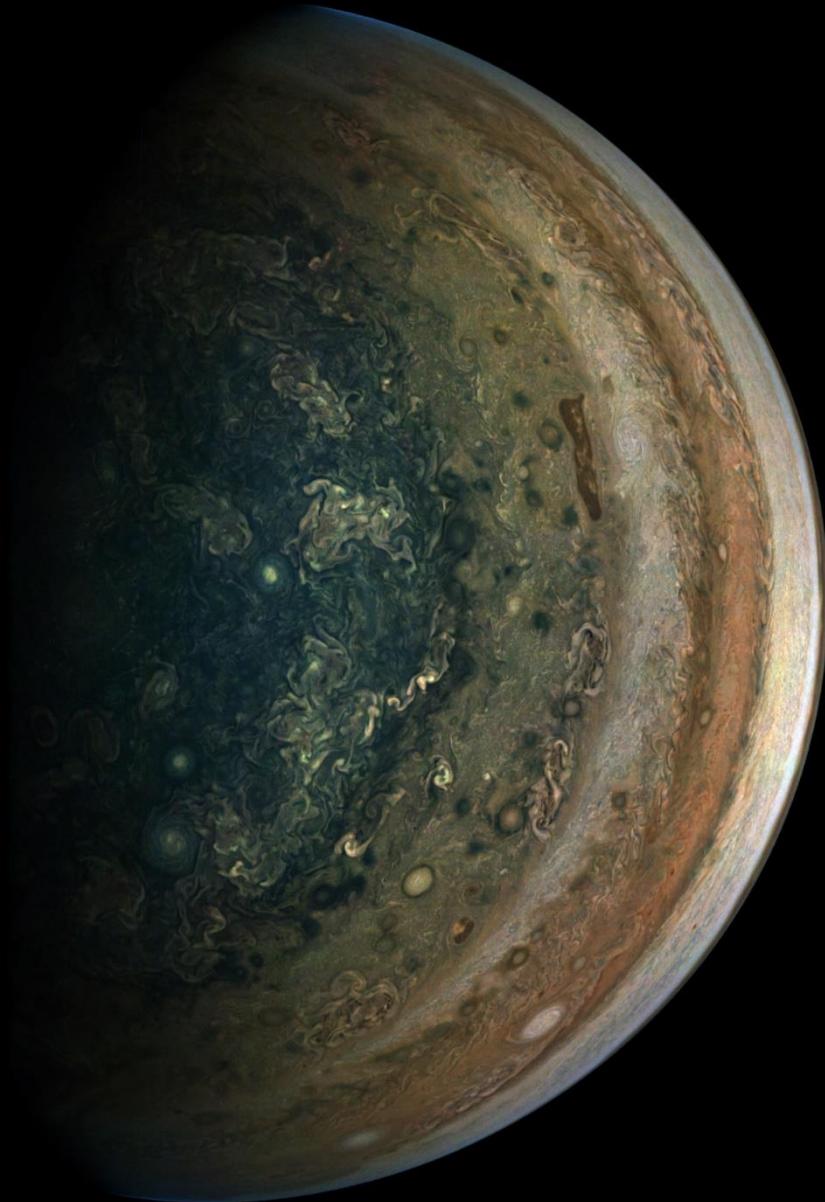
Cold-gas Jet Thruster

Poor performance
 I_{sp} : 24 s



Reliability
Simplicity

Xenon-cold-gas thruster



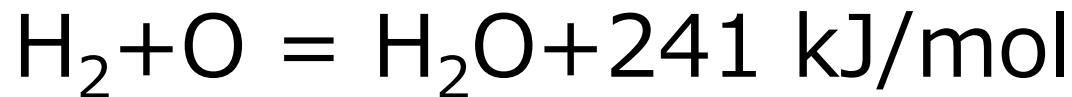
1: Fundamentals

2: Chemical Propulsion

3: Electric Propulsion

4: Micropropulsion

CP (Chemical E → Kinetic E)



18 g

$$\frac{1}{2} \dot{m} u_e^2 = E$$

$$\rightarrow u_e = 5 \text{ km/s}$$

Mass & energy are coupled → Velocity limit
Actual limit: about 4.5 km/s

EP

(Electrical E → Kinetic E)

Energy



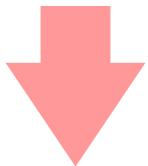
Arbitrarily

Propellant

No velocity limit



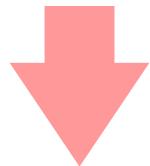
Exhaust velocity can be increased
by electric propulsion



Possible:

Over 90% payload for $\Delta V = 10 \text{ km/s}$
(e.g. 100 km/s propulsion for Jupiter)

But, it's not an all-rounder



Small thrust (~ 0.1 N)

Long operation time (~ 1 year)

By solar array panel
(limited)

$$\eta P = \frac{1}{2} \dot{m} u_e^2$$



Energy conversion eff.

Energy conservation

By solar array panel
(limited)

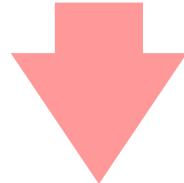
$$\eta P = \frac{1}{2} \dot{m} u_e^2 = \frac{1}{2} \underline{F u_e}$$

Energy conversion eff.

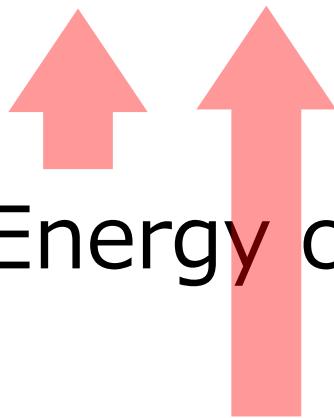
Constant

High velocity &
Low thrust

By solar array panel
(limited)



$$\eta PT = \frac{1}{2} Fu_e T = \frac{1}{2} M_{sc} \Delta V u_e$$



Operation time

High velocity &
Long time

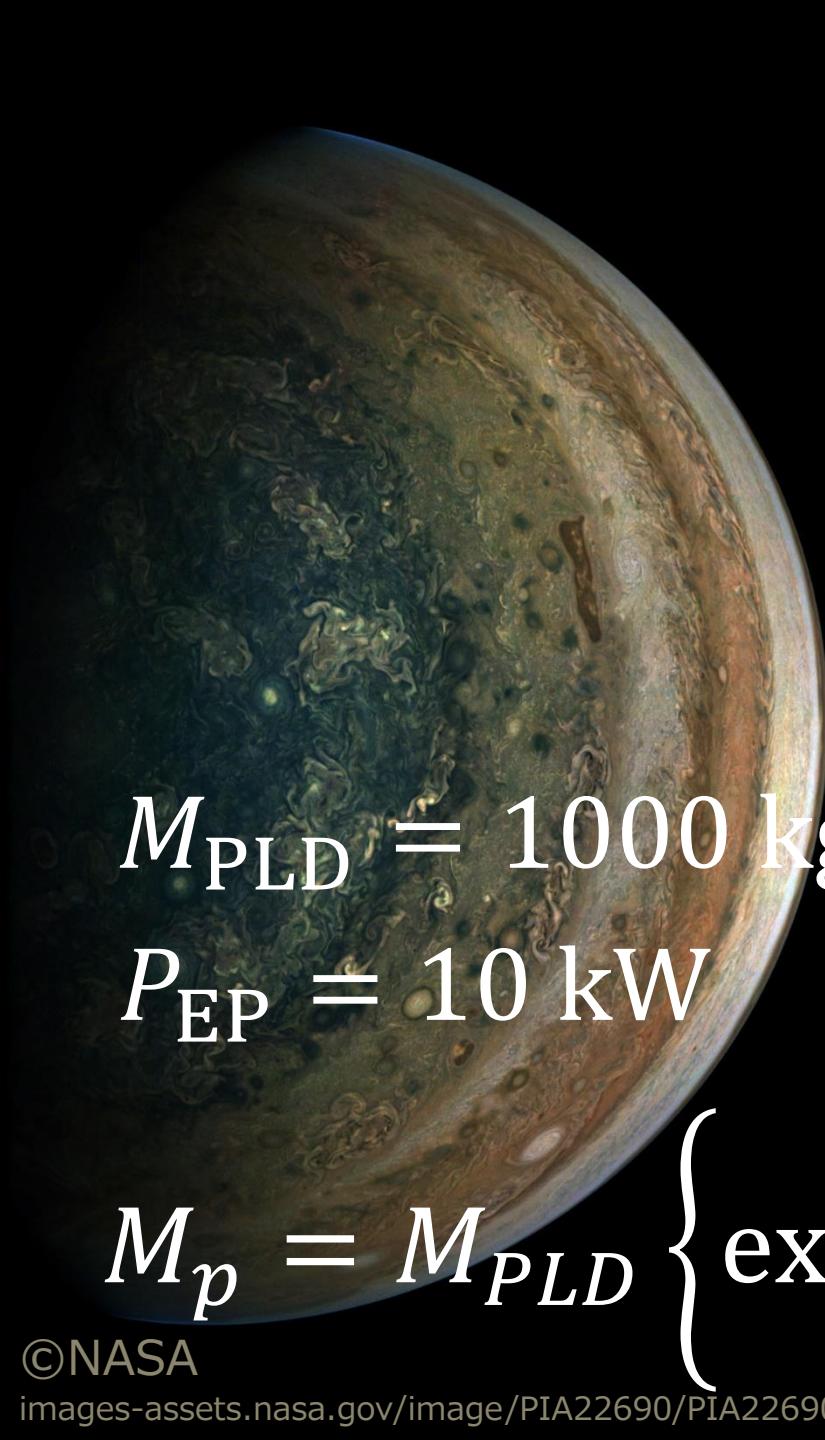
Q: Higher ex. velocity, better?

A : NO

Why ?

If the available power is limited,
the operation time is too long.

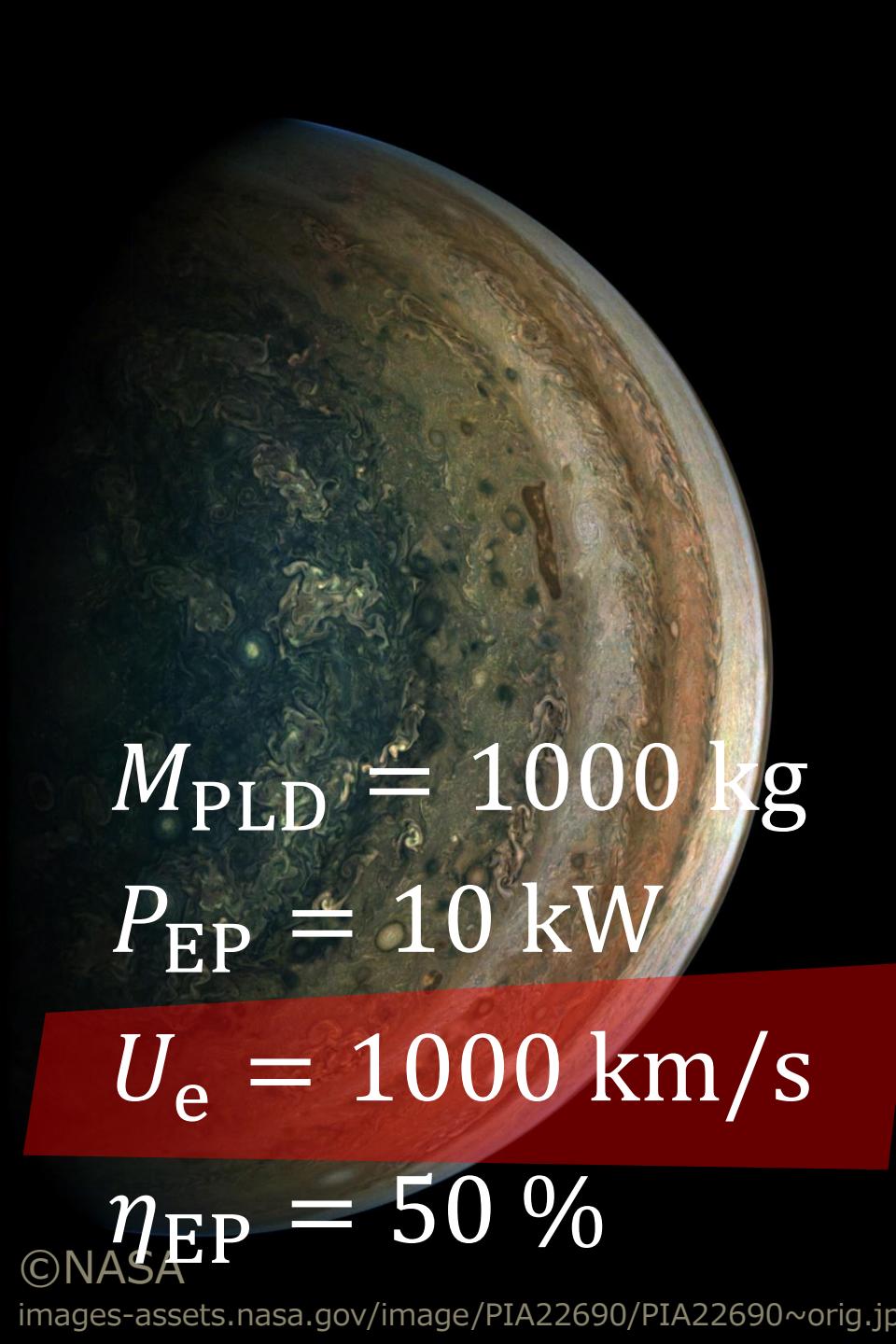
$$\Delta V = 13 \text{ km/s}$$


$$M_{PLD} = 1000 \text{ kg}$$

$$P_{EP} = 10 \text{ kW}$$

$$M_p = M_{PLD} \left\{ \exp \left(\frac{\Delta V}{u} \right) - 1 \right\}$$

$$\Delta V = 13 \text{ km/s}$$


$$M_{\text{PLD}} = 1000 \text{ kg}$$

$$P_{\text{EP}} = 10 \text{ kW}$$

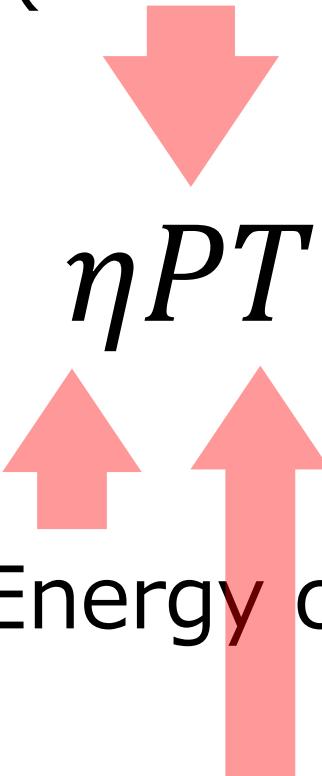
$$U_e = 1000 \text{ km/s}$$

$$\eta_{\text{EP}} = 50 \%$$

©NASA

images-assets.nasa.gov/image/PIA22690/PIA22690~orig.jpg

By solar array panel
(limited)



$$\eta PT = \frac{1}{2} Fu_e T = \frac{1}{2} M_{sc} \Delta V u_e$$

Energy conversion eff.

Operation time

High velocity &
Long time

$$M_{\text{PLD}} = 1000 \text{ kg}$$

$$P_{\text{EP}} = 10 \text{ kW}$$

$$U_e = 1000 \text{ km/s}$$

$$\eta_{\text{EP}} = 50 \text{ \%}$$

$$F_{\text{EP}} = 10 \text{ mN}$$

$$\dot{m}_{EP} = 10 \text{ } \mu\text{g/s}$$

$$M_{\text{EP}} = 13 \text{ kg}$$

$$\tau_{\text{EP}} = 41 \text{ year}$$

$$M_{\text{PLD}} = 1000 \text{ kg}$$

$$P_{\text{EP}} = 10 \text{ kW}$$

$$U_e = 30 \text{ km/s}$$

$$\eta_{\text{EP}} = 50 \text{ \%}$$

$$F_{\text{EP}} = 0.3 \text{ N}$$

$$\dot{m}_{EP} = 10 \text{ mg/s}$$

$$M_{\text{EP}} = 542 \text{ kg}$$

$$\tau_{\text{EP}} = 1.5 \text{ year}$$

$$M_{\text{PLD}} = 1000 \text{ kg}$$

$$P_{\text{EP}} = 1000 \text{ W}$$

$$U_e = 10 \text{ km/s}$$

$$\eta_{\text{EP}} = 50 \text{ \%}$$

$$F_{\text{EP}} = 1 \text{ N}$$

$$\dot{m}_{EP} = 0.1 \text{ g/s}$$

$$M_{\text{EP}} = 2670 \text{ kg}$$

$$\tau_{\text{EP}} = 0.8 \text{ year}$$

$$M_{\text{PLD}} = 1000 \text{ kg}$$

By CP

$$U_e = 2.5 \text{ km/s}$$



$$M_{\text{EP}} = 180,000 \text{ kg}$$

Operation time: 10 min.

Flying time: 2-6 years

Q: Higher ex. velocity, better?

A : NO

Why ?

Even if you increase the power to shorten the operation time,
Solar array mass increases more than the propellant reduction.

$$M_{\text{PLD}} = 1000 \text{ kg}$$

$$P_{\text{EP}} = 10 \text{ kW}$$

$$U_e = 30 \text{ km/s}$$

$$\eta_{\text{EP}} = 50 \text{ \%}$$

$$F_{\text{EP}} = 0.3 \text{ N}$$

$$\dot{m}_{EP} = 10 \text{ mg/s}$$

$$M_{\text{EP}} = 542 \text{ kg}$$

$$\tau_{\text{EP}} = 1.5 \text{ year}$$

$$M_{\text{PLD}} = 1000 \text{ kg}$$

$$P_{\text{EP}} = 300 \text{ kW}$$

$$U_e = 1000 \text{ km/s}$$

$$\eta_{\text{EP}} = 50 \text{ \%}$$

$$F_{\text{EP}} = 0.3 \text{ N}$$

$$\dot{m}_{EP} = 0.3 \text{ mg/s}$$

$$M_{\text{EP}} = 13 \text{ kg}$$

$$\tau_{\text{EP}} = 1.4 \text{ year}$$



Solar array mass : 30-50 W/kg

→ 100 kW & 3000 kg

$$M_{\text{PLD}} = 1000 \text{ kg}$$

$$P_{\text{EP}} = 300 \text{ kW}$$

$$U_e = 1000 \text{ km/s}$$

$$\eta_{\text{EP}} = 50 \text{ \%}$$

$$F_{\text{EP}} = 0.3 \text{ N}$$

$$\dot{m}_{EP} = 0.3 \text{ mg/s}$$

$$M_{\text{EP}} = 13 \text{ kg}$$

$$\tau_{\text{EP}} = 1.4 \text{ year}$$

$$M_{\text{SAP}} = 9,900 \text{ kg}$$

Optimum exhaust velocity

$$\text{Thrust Efficiency } \eta_{\text{th}} = \frac{\dot{m}_{\text{prop}} V_e^2}{2P_s}$$

P_s : Available Power

Specific power of solar cell panels

$$a = P_s / m_{\text{panel}} \text{ (W/kg)}$$

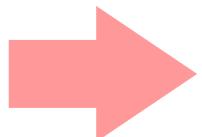
$$\beta = m_{\text{panel}} / P_s \text{ (kg/W)}$$

Typical $\beta = 0.05 \text{ kg/W}$

Propellant consumption rate

$$\dot{m}_{\text{prop}} = m_{\text{prop}} / \tau$$

τ : Transfer Time



$$m_i = m_{\text{pay}} + \beta P_s + \dot{m}_{\text{prop}}$$

Optimum exhaust velocity

$$\frac{m_{\text{pay}}}{m_i} = 1 - \frac{\beta P_s}{m_i} - \frac{m_{\text{prop}}}{m_i}$$

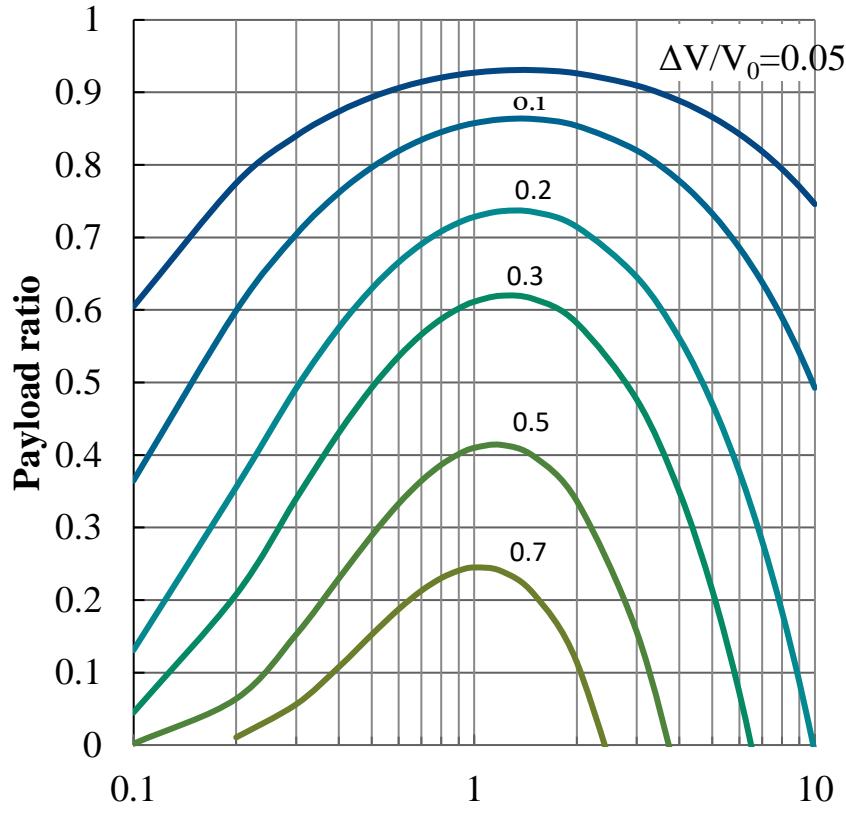
$$= 1 - \frac{m_{\text{prop}}}{m_i} \left(\frac{\beta P_s}{\dot{m}_{\text{prop}} \tau} + 1 \right)$$

$$= 1 - \left(1 - \exp \left(\frac{-\Delta V}{V_e} \right) \right) \left(\frac{\beta V_e^2}{2\eta_{\text{th}} \tau} + 1 \right)$$

$$= \exp \left(\frac{-\Delta V}{V_e} \right) - \frac{\beta V_e^2}{2\eta_{\text{th}} \tau} \left\{ 1 - \exp \left(\frac{-\Delta V}{V_e} \right) \right\}$$

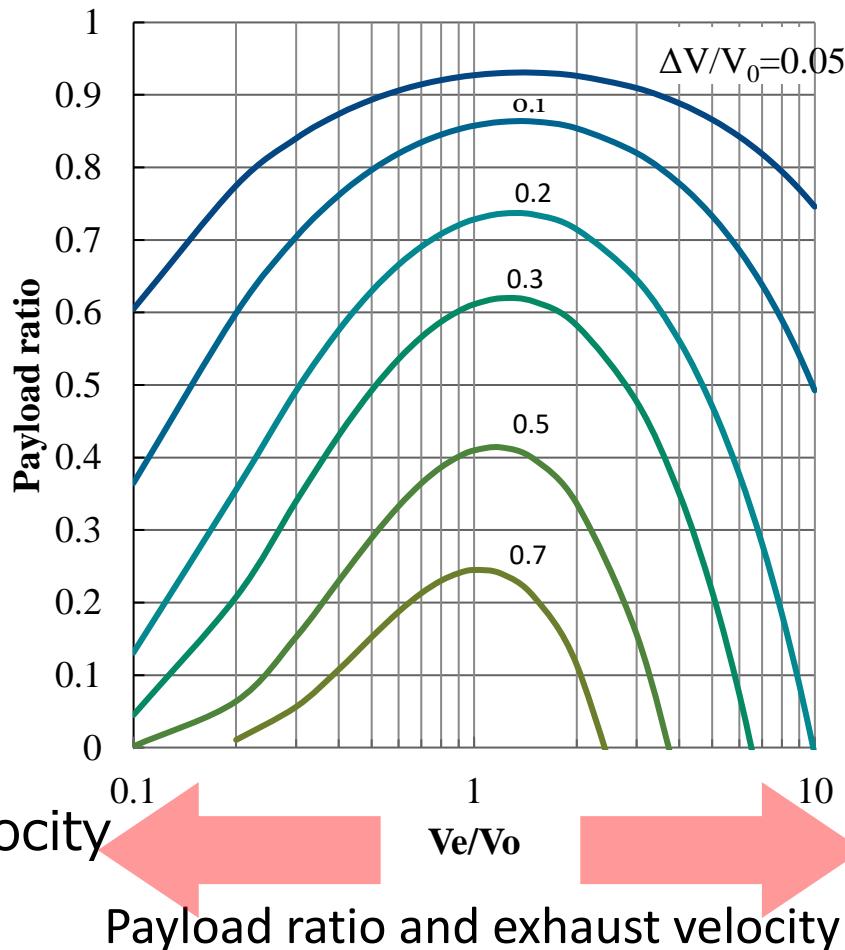
$$V_{e,\text{opt}} \approx V_0 = \sqrt{\eta_{\text{th}} \tau / \beta}$$

$V_{e,\text{opt}} \approx 10 \text{ km/s}$ for 30 days, 33 km/s for 1 year.



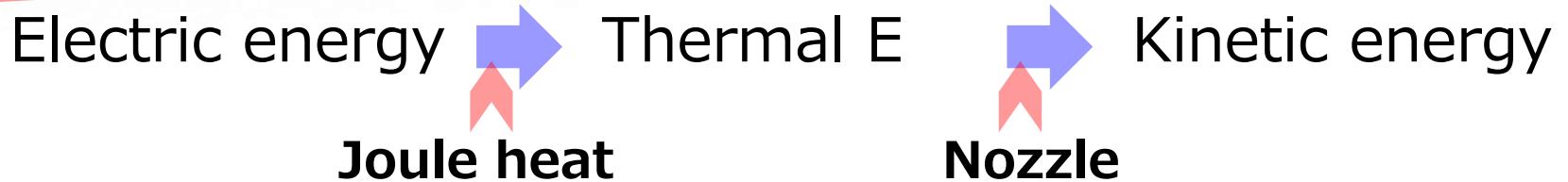
Payload ratio and exhaust velocity

Optimum exhaust velocity



Category of EP

ETA: Eletrothermal Acceleration



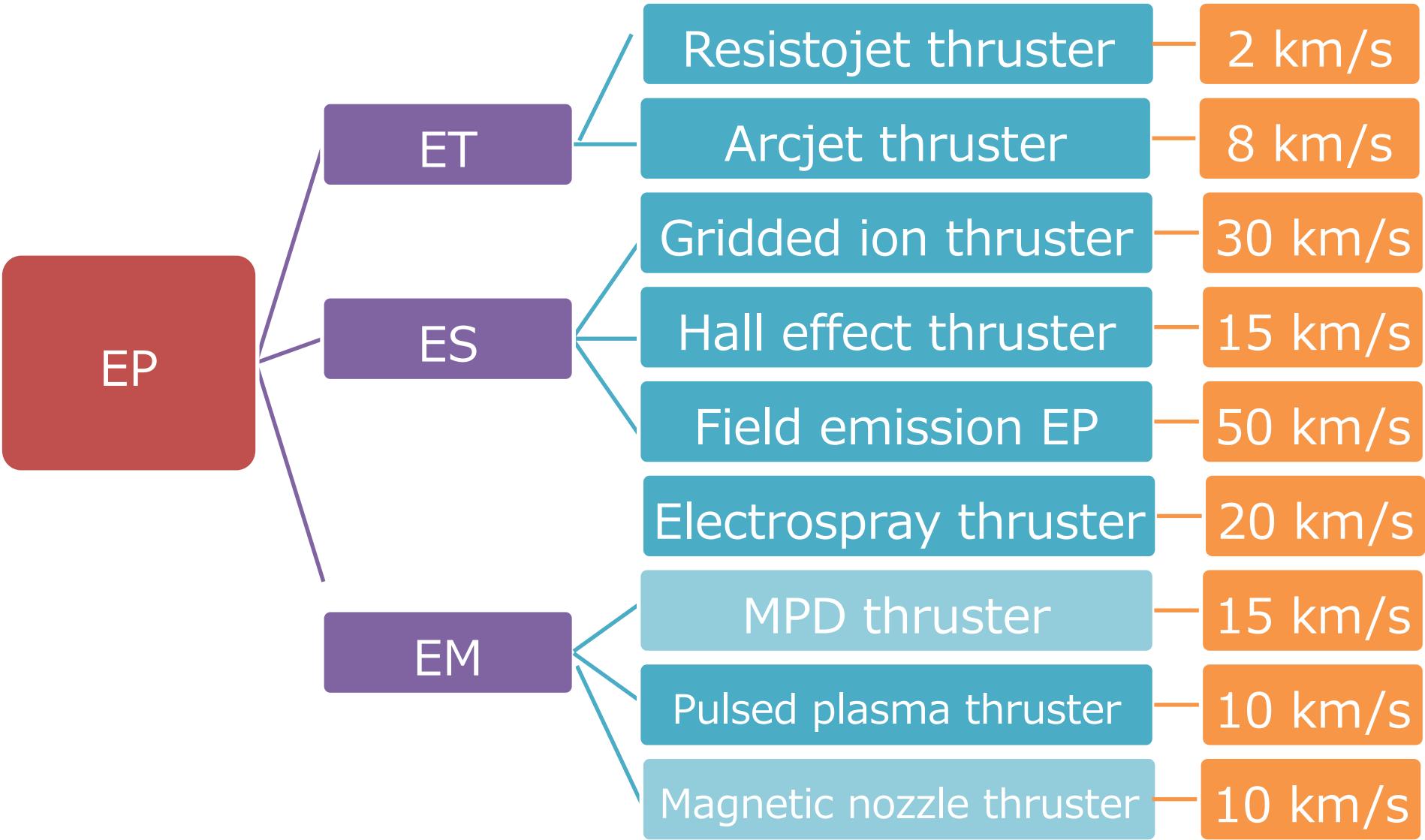
ESA: Electrostatic Acceleration



EMA: Electromagnetic Acceleration



EP Thrusters



Resistojet thruster

Application: many

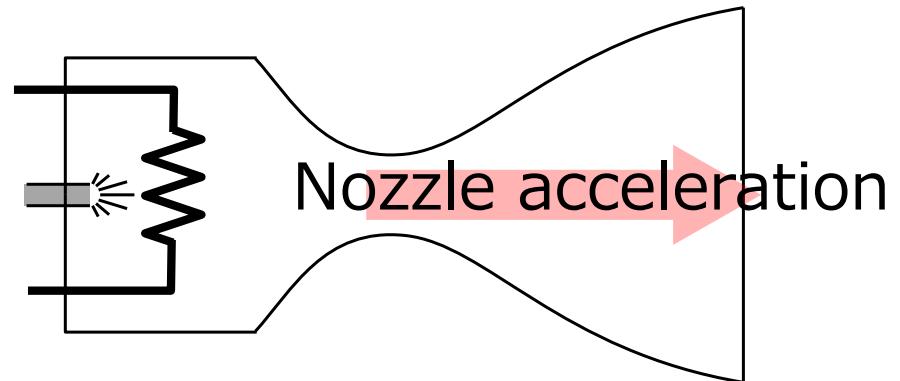
Working fluid: hot gas

W.F. generation: resistive heating

Acceleration: nozzle

Exhaust velocity (typical): 1 – 5 km/s

Power (typical): 10 W – 2 kW



Arcjet thruster

Application: many

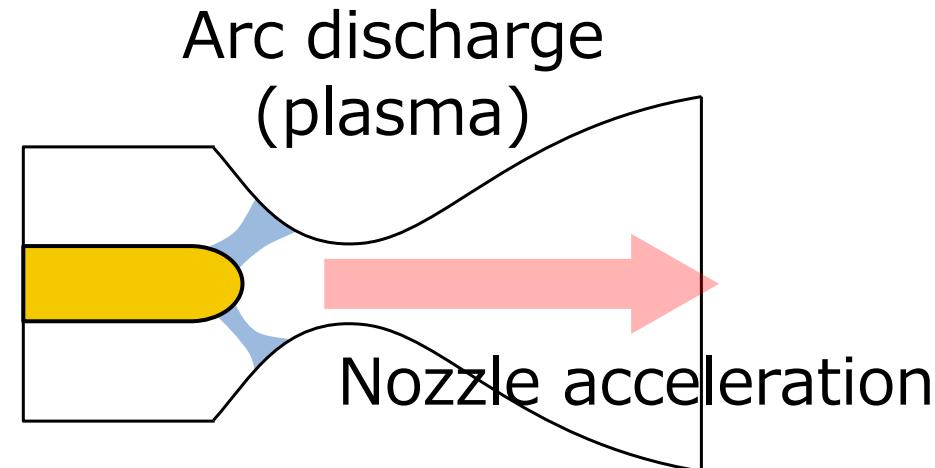
Working fluid: plasma

W.F. generation: arc discharge

Acceleration: nozzle

Exhaust velocity (typical): 5 – 10 km/s

Power (typical): 1 – 2 kW



Gridded ion thruster

Application: many

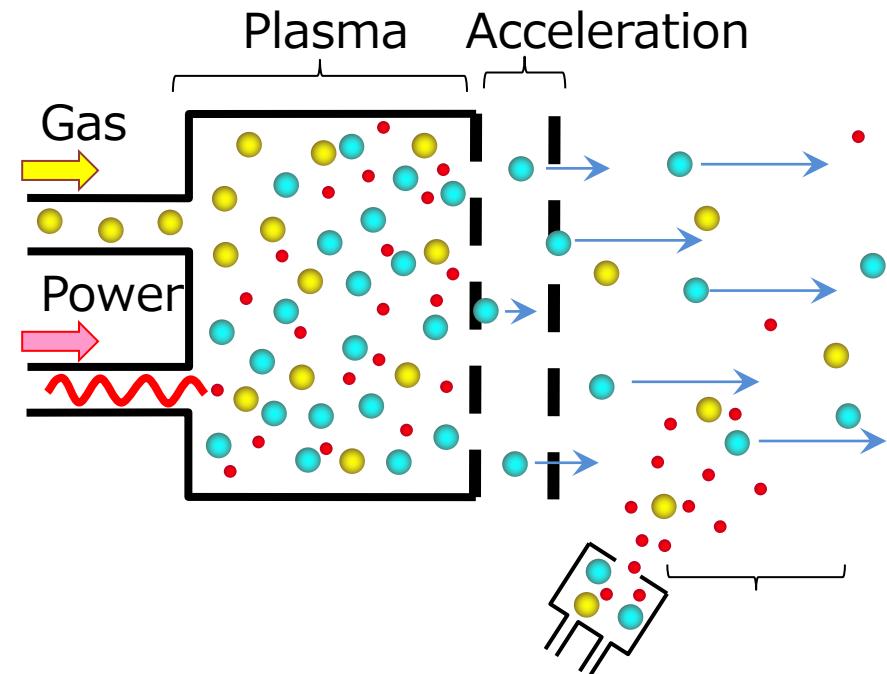
Working fluid: plasma

W.F. generation: DC-discharge, RF, microwave

Acceleration: Electrostatic, 1 kV

Exhaust velocity (typical): 30 km/s

Power (typical): 0.5 – 2.0 kW



Hall effect thruster

Application: many

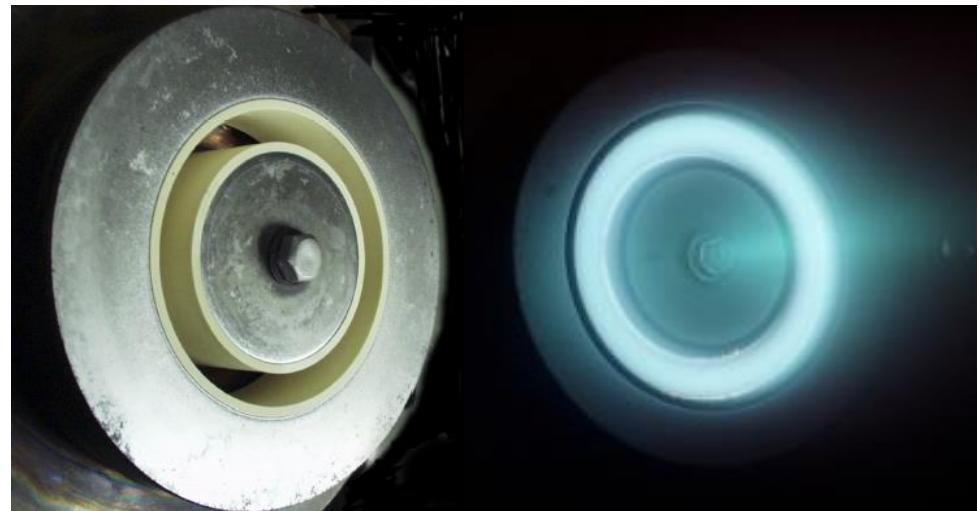
Working fluid: plasma

W.F. generation: DC-discharge

Acceleration: Electrostatic, 300 V

Exhaust velocity (typical): 15 km/s

Power (typical): 0.5 – 2.0 kW



Field emission electric propulsion

Application: 20 in space

Working fluid: ionized liquid metal

W.F. generation: field emission

Acceleration: Electrostatic, 10 kV

Exhaust velocity (typical): 50 km/s

Power (typical): 40 W

Electrospray thruster

Application: a few demonstrations

Working fluid: ionized/droplet ionic liquid

W.F. generation: field emission/Tayler-cone

Acceleration: electrostatic, 1-3 kV

Exhaust velocity (typical): 10-20 km/s

Power (typical): 5 W

Pulsed plasma thruster

Application: several demonstrations

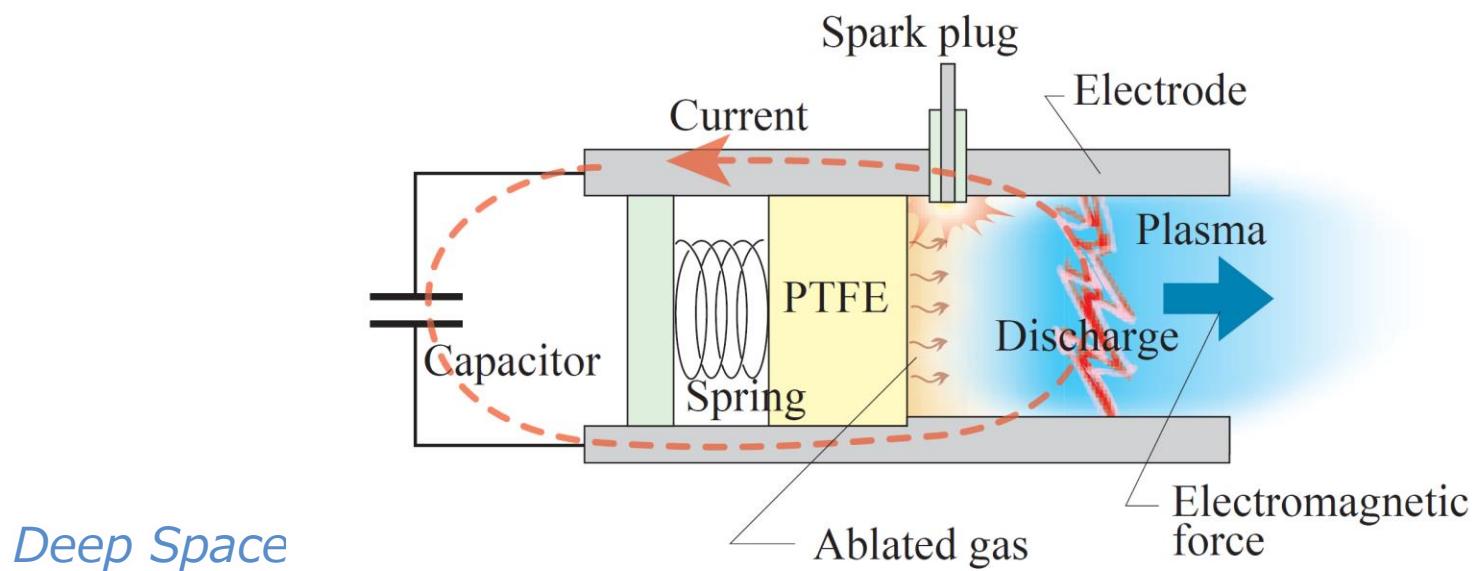
Working fluid: plasma

W.F. generation: pulsed arc discharge

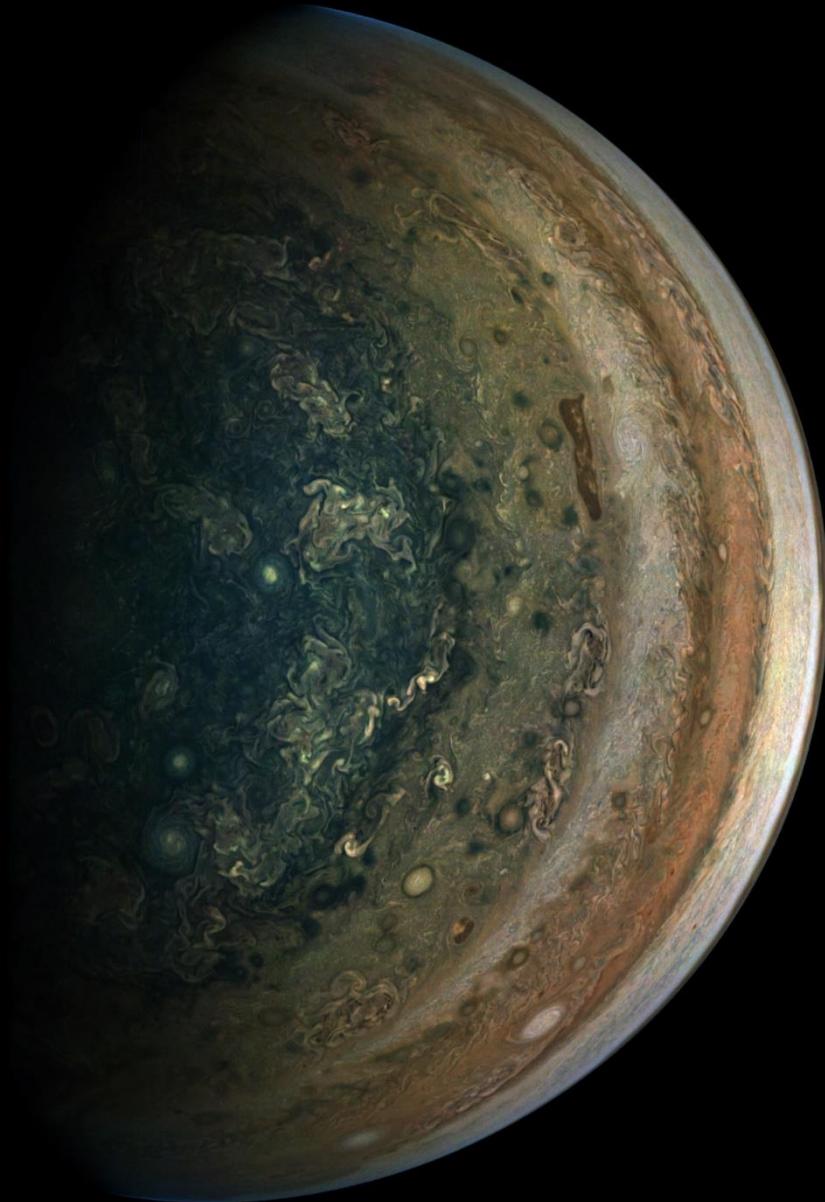
Acceleration: electromagnetic/electrothermal, 1-3 kV

Exhaust velocity (typical): 5-20 km/s

Power (typical): 10 W



Deep Space



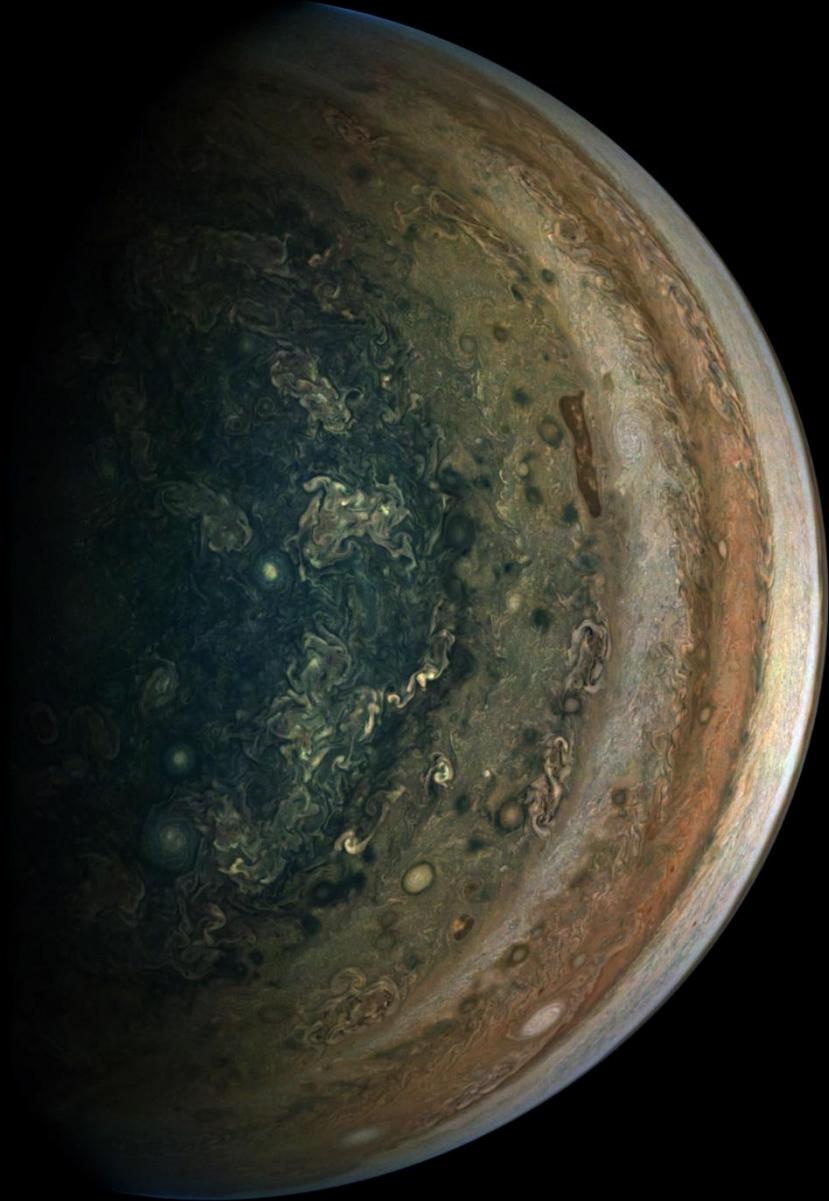
- 1: Fundamentals
 - 2: Chemical Propulsion
 - 3: Electric Propulsion
 - 4: Micropropulsion**
-
-
-

What is micropropulsion?



Just Small

There are difficulties in miniaturization of technology. The performance becomes lower (it's nature, unavoidable). If you are a developer, it's a big challenge, but if you are a user, what you do is to select the suitable one.



1: Fundamentals
2: Chemical Propulsion
3: Electric Propulsion

4: Micropropulsion

-
- 4.A: Key words
 - 4.B: How to choose?
 - 4.C: Recent trend
 - 4.D: Pickup

1. Different roles

I. High specific impulse

Orbit transfer

Drag compensation

II. Multiaxis thrust

Unloading

Rendezvous

III. High thrust

Insertion
Escaping

Landing

Emergency

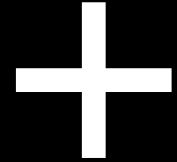
Miniaturization as system

Still small-satellites have little resource

2.Unified propulsion

PROCYON:

Ion thruster

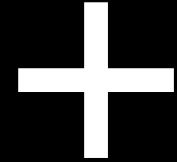


Cold-gas thruster

By gas-sharing

ArgoMoon:

Green-mono



Cold-gas thruster

By plenum-gas usage

3. Safety

Xenon
2.3 kg

High-pressure
gas system (dry)

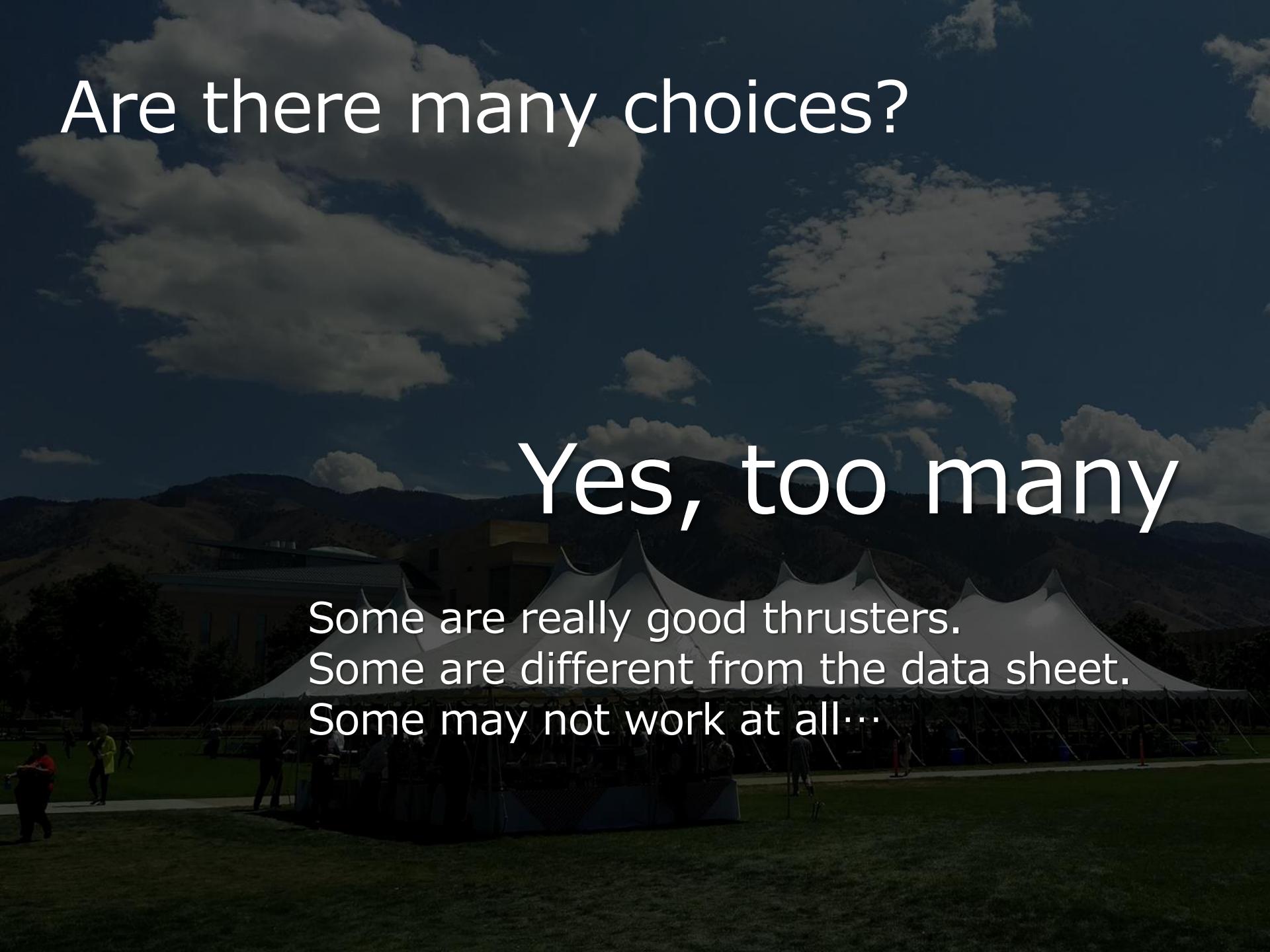
4.5 kg

vs. Regulation



vs. Safety review



The background of the slide is a dark, atmospheric photograph of a field under a cloudy sky. In the foreground, there are several white tents and a few people walking around.

Are there many choices?

Yes, too many

Some are really good thrusters.

Some are different from the data sheet.

Some may not work at all…

Which should you choose?

Enough information?

- ✓ NOT only performance, but principle, photo, dimensions, etc. are important.
- ✓ Is that principle feasible?
- ✓ Was it measured? How?
- ✓ Do they publish it at conferences/journals?

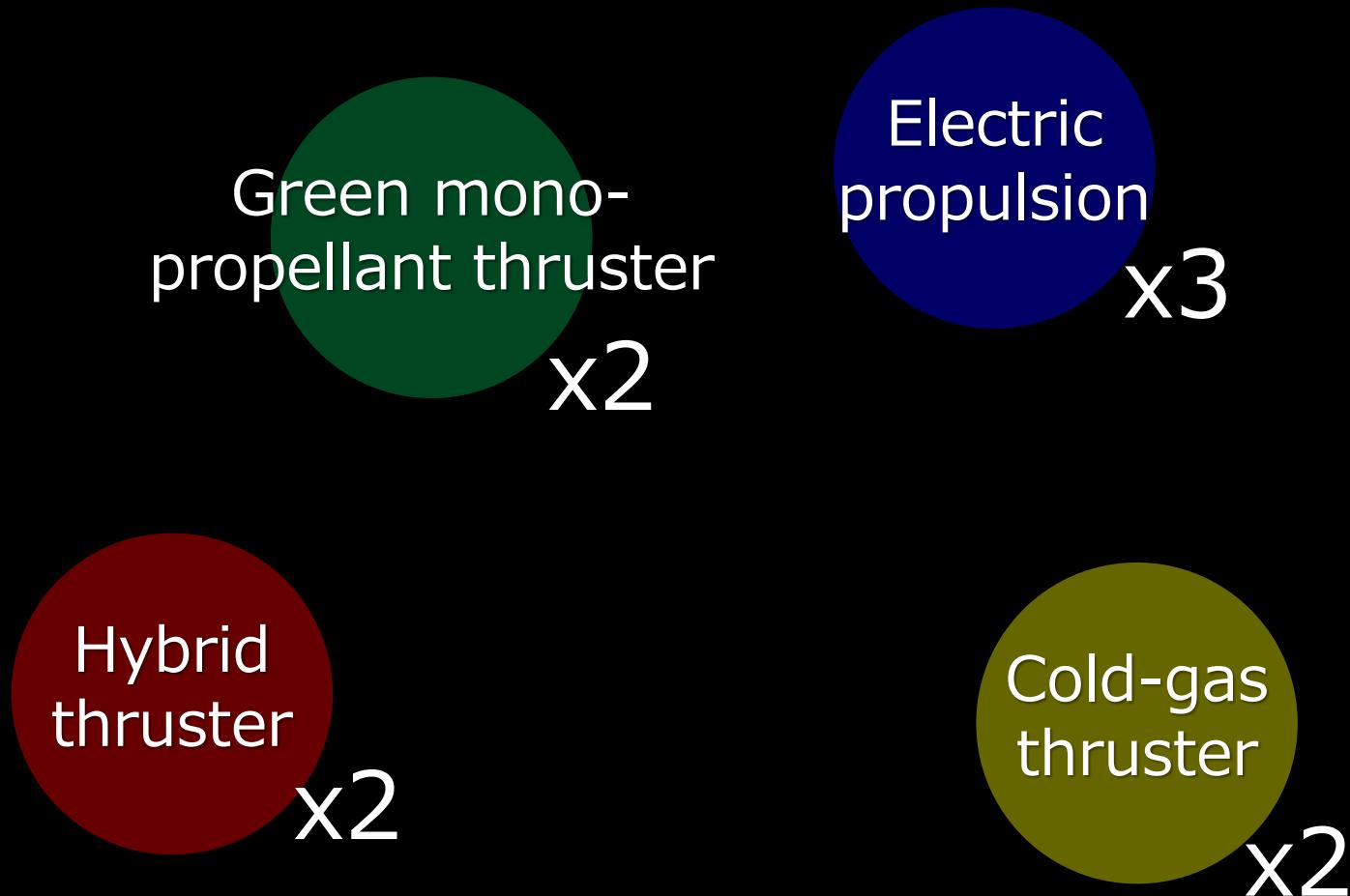


What is getting attention ?

The best place to check the trend of small satellites:
Small Satellite Conference

- ✓ More industry side rather than academic
- ✓ Single-session presentation & huge exhibition
 - ✓ ⇒ Severe selection ⇒ good index
- ✓ SSC2020 was online

Propulsion topics at SSC-2019/2020



Propulsion topics at SSC-2019/2020

- ✓ High thrust
- ✓ Safety

Green mono-propellant thruster

x2

- ✓ High thrust
- ✓ Safety

Hybrid thruster

x2

- ✓ High ΔV
- ✓ Safety

Electric propulsion

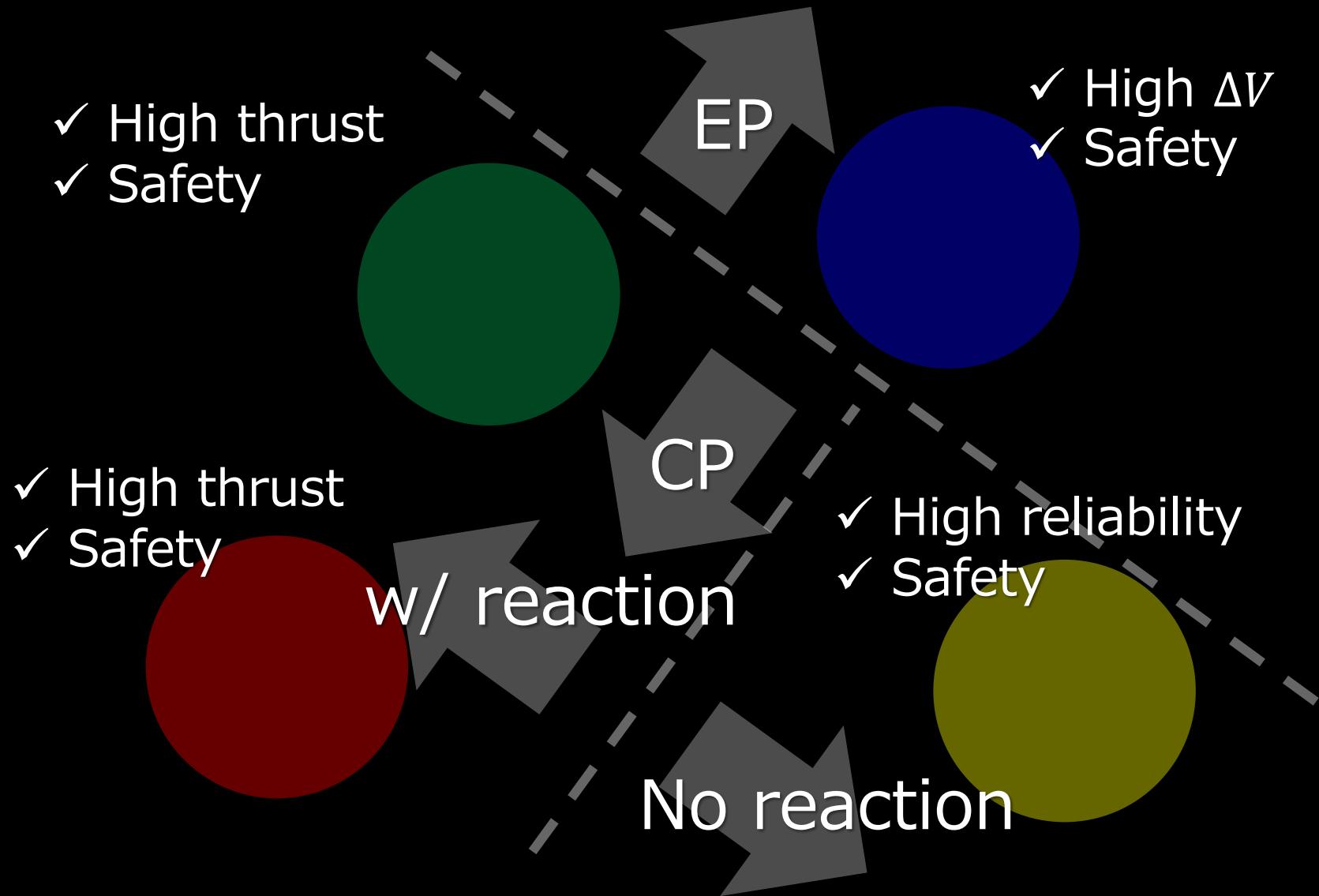
x3

- ✓ High reliability
- ✓ Safety

Cold-gas thruster

x2

Different ability by different type



“Safety” is the KEY

- ✓ High thrust
 - ✓ Safety
-

Green mono-propellant thruster

- ✓ High thrust
 - ✓ Safety
-

Hybrid thruster

✓ High ΔV
✓ Safety

Electric propulsion

- ✓ High reliability
 - ✓ Safety
-

Cold-gas thruster

Degree of “Safety” is different

- AF-M315E = NH_3OHNO_3 , etc
- LMP-103S = $\text{NH}_4(\text{NO}_2)_2\text{N}$, etc
- ✓ Safety

Green mono-propellant thruster

✓ Safety

Hybrid thruster

- ABS + Gas O₂
- ABS + O₂/N₂O

✓ Safety
Electric propulsion

- Water
- Teflon
- Indium

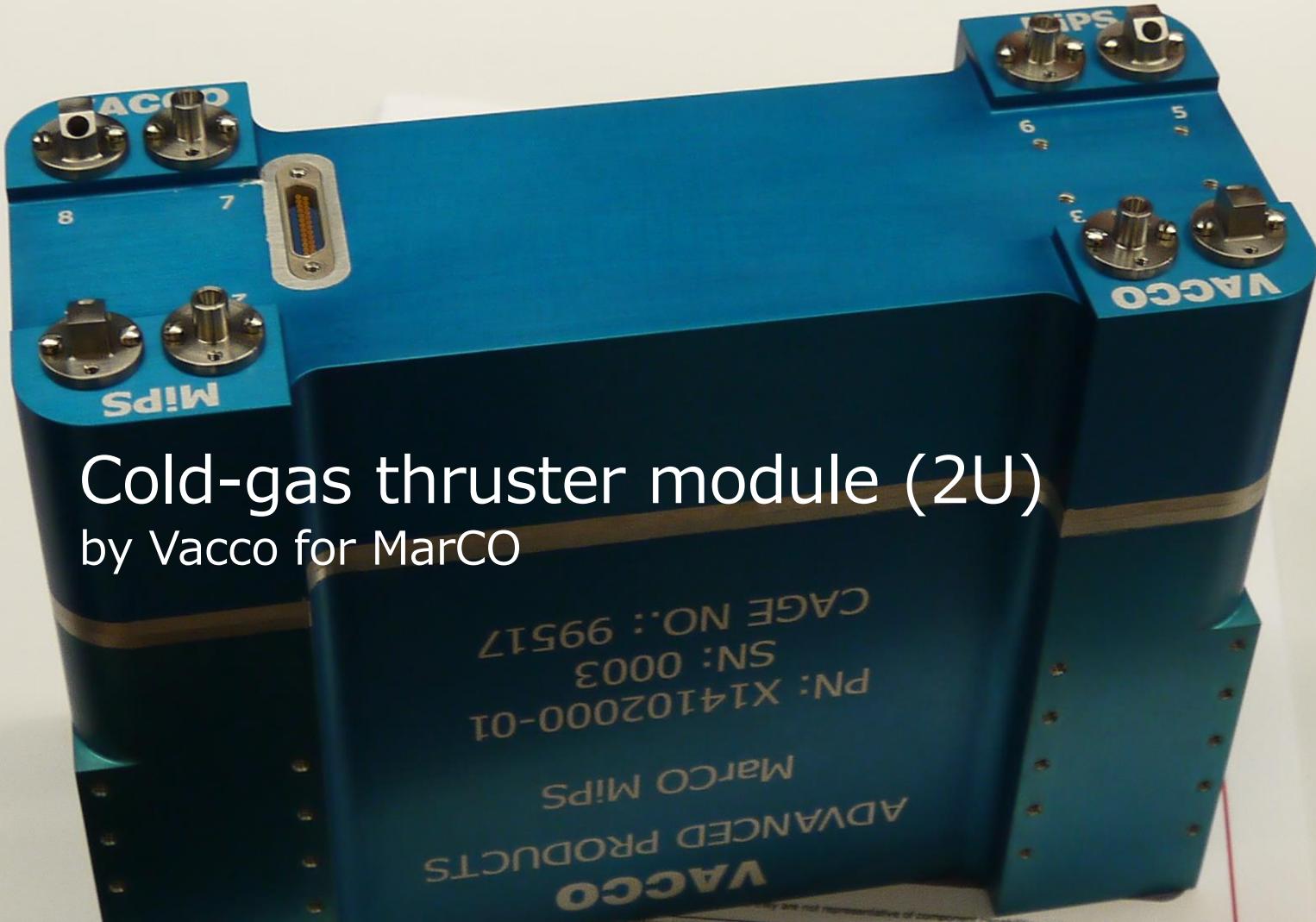
✓ Safety

Cold-gas thruster

- Indium
- Pressurized gas

MarCO

has a multiaxis-thruster system using cold-gas (R134a).



FEEP

By ENPULSION

- Indium
- 0.9 kg, 40 W, 5000 Ns, 0.35 mN, 2000 s
- Operation in 2018 April !!



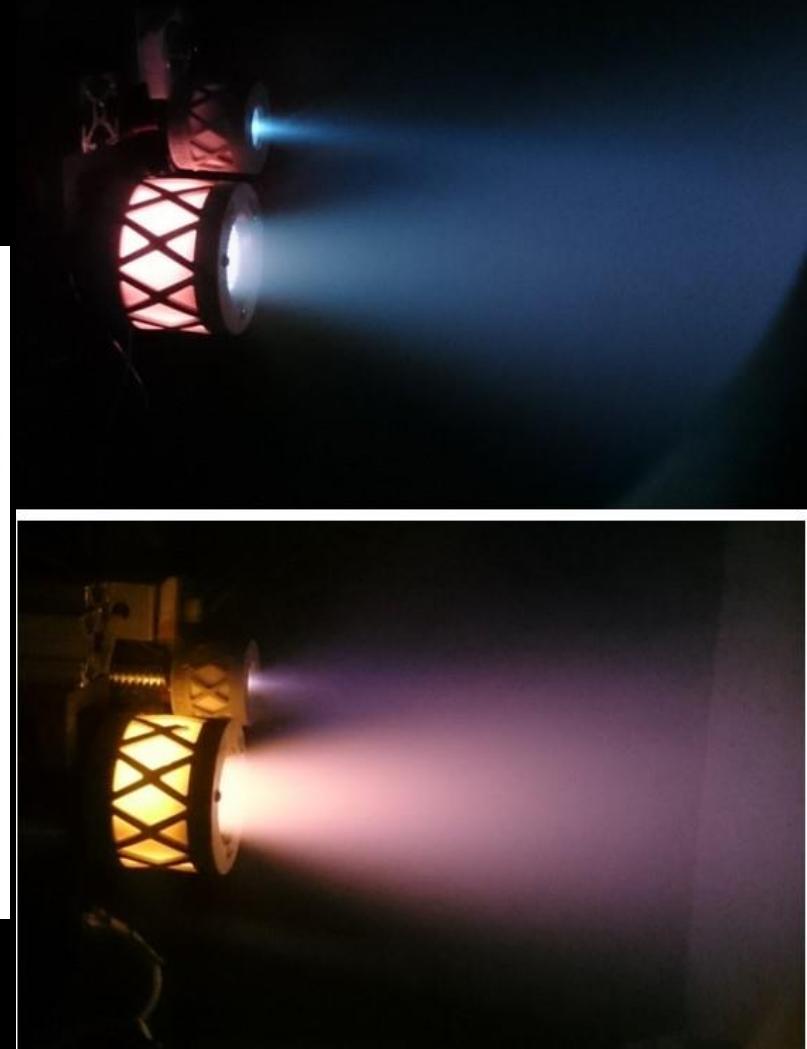
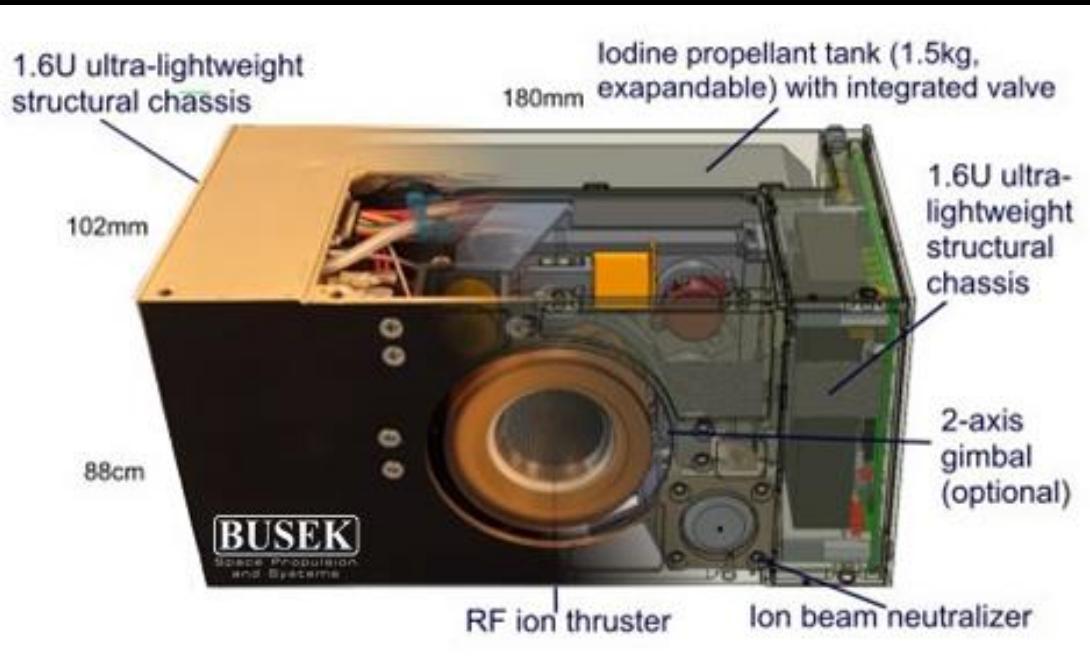
ENPULSION NANO

Image courtesy of ENPULSION©, All rights reserved.

Iodine ion thruster; BIT-3

By Busek Co. Inc.

- iodine
- 3.0 kg, 80 W, 40000 Ns, 1.24 mN, 2600 s
- Planned in 2019 by SLS-EM1

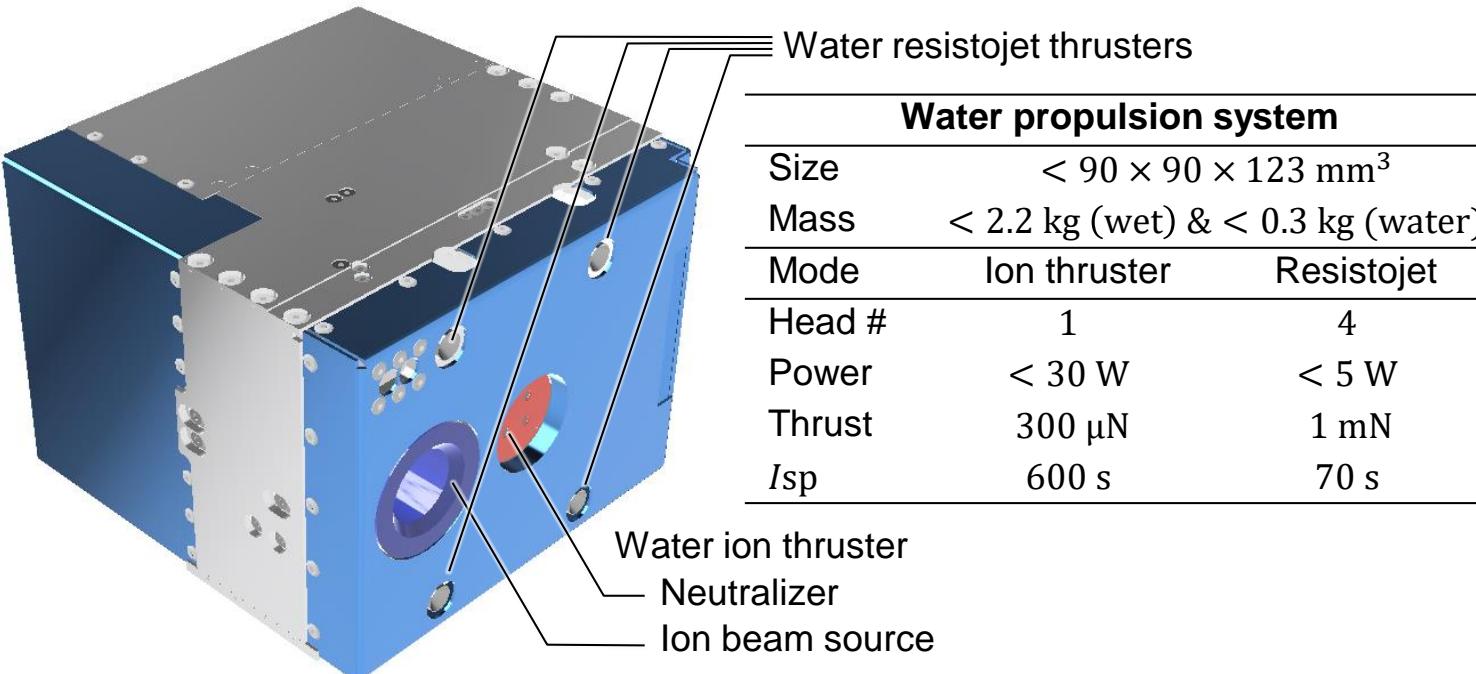


(C) BUSEK

Water Unified Propulsion

By Pale Blue Inc.

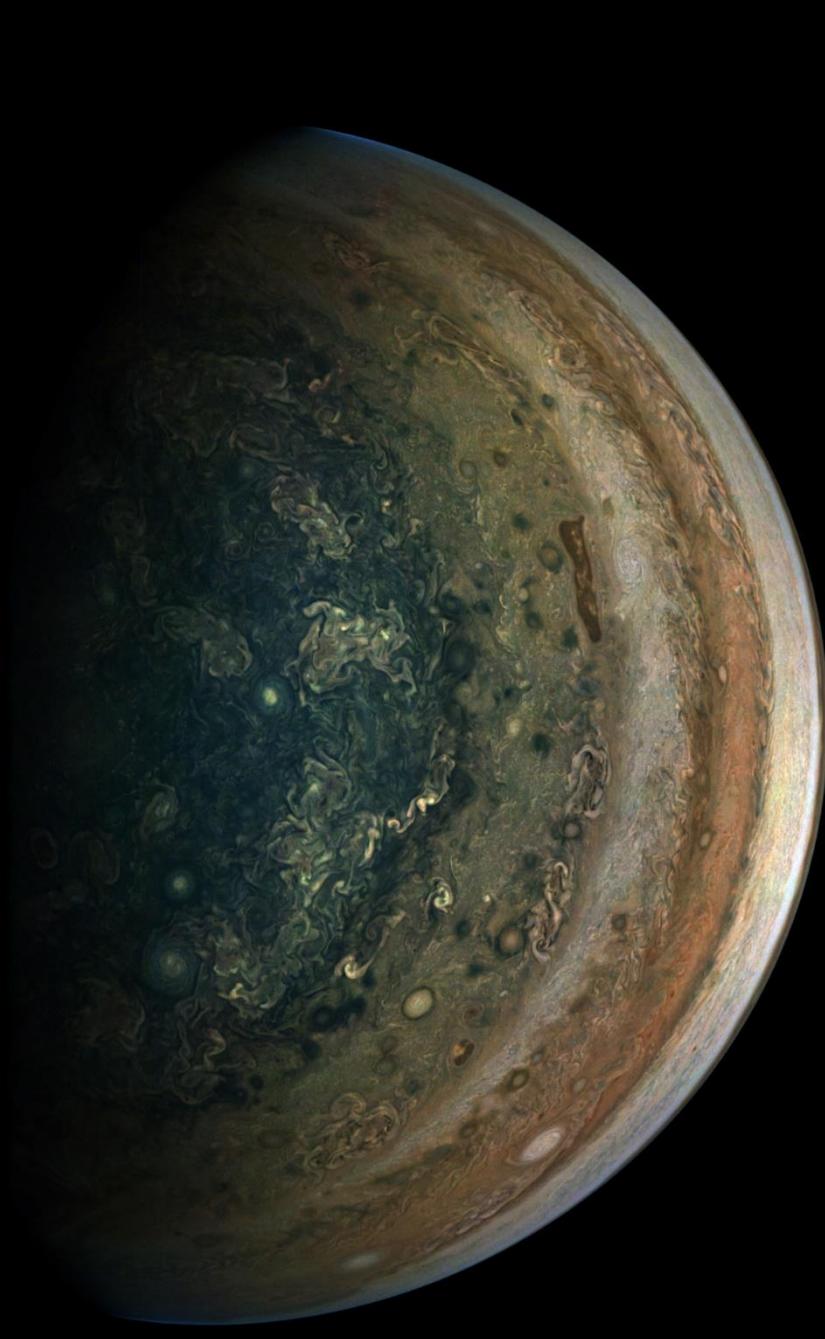
- Water ion thruster & Water Resistojet thruster
- Size $90 \times 90 \times 123 \text{ mm}^3$, $< 2.2 \text{ kg}$, Water $< 0.3 \text{ kg}$
- IT: $300 \mu\text{N}$, 600 s , T: 1 mN , $70 \text{ s} \times 4$
- Planned in 2022 by JAXA Innovative Program-3



Thruster name	Size	N	Total Impulse		Power W
			U	-	
Aerospace MEMS	0.18	5			7
U of Texas Custom	0.40	1			56
SFL CNAPS	1.58	4			106
M IT SiEPS	0.20	1			116
Busek BET-100	0.40	1			175
Busek μ -resisto jet	4.00	4			8
Busek μ PPT	0.50	1			240
GW U μ CAT	0.20	4			252
Vacco MarCO prop.	1.50	8			570
CUA/Vacco CHIPS	1.60	1			755
Hyperion PM 200	1.00	1			814
Aerojet RD MPS-130	1.00	4			511
Tethers U HYDROS-C	2.00	1			920
Phase Four RFT	1.00	1			1200
Enpulsion IFM Nano T	1.00	1			2150
U of Tokyo Unified Water	3.00	1			2200
Busek BIT-3	1.60	4			40
		1			5100
		4			870
		1			20600
		4			56

Thruster name	Size U	N	Propellant	Thrust m N	
				-	-
Aerospace MEMS	0.18	5	HFC236fa		100.0
U of Texas Custom	0.40	1	HFC236fa		110.0
SFL CNAPS	1.58	4	SF ₆		50.0
M IT SiEPS	0.20	1	EM I-BF ₄		0.1
Busek BET-100	0.40	1	EM I-Im		0.1
Busek μ -resisto jet	4.00	4	Ammonia		0.5
Busek μ PPT	0.50	1	PTFE		0.5
GW U μ CAT	0.20	4	Nickel		0.0
Vacco MarCO prop.	1.50	8	HFC236fa		25.0
CUA/Vacco CHIPS	1.60	1	R134a		30.0
Hyperion PM 200	1.00	1	Propane/N ₂ O		500.0
Aerojet RD MPS-130	1.00	4	AF-M 315E		1.3
Tethers U HYDROS-C	2.00	1	Water		1.2
Phase Four RFT	1.00	1	Xenon		5.2
Enpulsion IFM Nano T	1.00	1	Indium		0.4
U of Tokyo Unified Water	3.00	1	Water		0.3
U of Tokyo Unified Water	3.00	4	Water		3.9
Busek BIT-3	1.60	1	Iodine		0.7

Thruster name		Size U	N -	Propellant	GHS #	NFPA		
						B	R	Y
Aerospace	MEMS	0.18	5	HFC236fa	4, 7	1	0	1
U of Texas	Custom	0.40	1	HFC236fa	4, 7	1	0	1
SFL	CNAPS	1.58	4	SF ₆	4	2	0	0
MIT	SiEPS	0.20	1	EM I-BF ₄	7	3	1	0
Busek	BET-100	0.40	1	EM I-Im	6	2	1	0
Busek	μ -resisto jet	4.00	4	Ammonia	4, 5, 7, 9	3	0	0
Busek	μ PPT	0.50	1	PTFE	NC	1	0	0
GWU	μ CAT	0.20	4	Nickel	2, 7, 8	2	1	0
Vacco	MarCO prop.	1.50	8	HFC236fa	4, 7	1	0	1
CUA/Vacco	CHIPS	1.60	1	R134a	4	2	1	0
Hyperion	PM 200	1.00	1	Propane/N ₂ O	2, 3, 4	2	4	0
Aerojet RD	MPS-130	1.00	4	AF-M 315E	1, 6, 7, 8	3	0	0
Tethers U	HYDROS-C	2.00	1	Water	NC	0	0	0
Phase Four	RFT	1.00	1	Xenon	4	0	0	0
Enpulsion	IFM Nano T	1.00	1	Indium	8	2	0	0
U of Tokyo	Unified Water	3.00	1	Water	NC	0	0	0
Busek	BIT-3	1.60	1	Iodine	5, 6, 7, 9	3	0	0



Thank you